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Numerical and semi-analytical structure-preserving model reduction for MEMS

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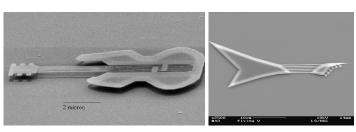


Collaborators

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Resonant MEMS

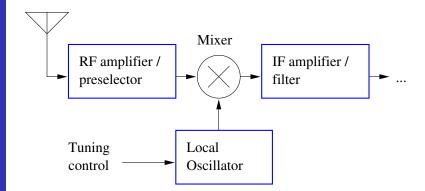
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Microguitars from Cornell University (1997 and 2003)

- MHz-GHz mechanical resonators
- Favorite application: radio on chip
- Close second: really high-pitch guitars

The Mechanical Cell Phone



- Your cell phone has many moving parts!
- What if we replace them with integrated MEMS?

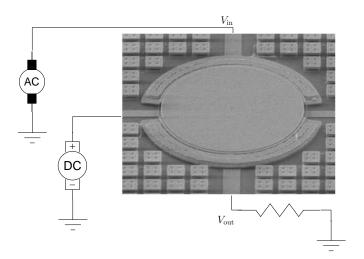


Ultimate Success

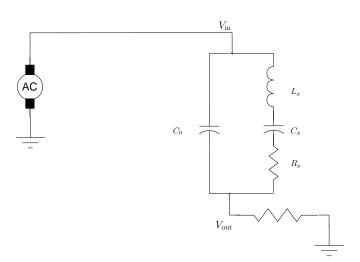
"Calling Dick Tracy!"



Example Resonant System



Example Resonant System



The Designer's Dream

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Ideally, would like

- Simple models for behavioral simulation
- Parameterized for design optimization
- Including all relevant physics
- With reasonably fast and accurate set-up

We aren't there yet.

The Hero of the Hour

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Major theme: use problem structure for better models

- ODE structure
- Complex symmetric structure
- Perturbative structure
- Geometric structure

SOAR and ODE structure

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Damped second-order system:

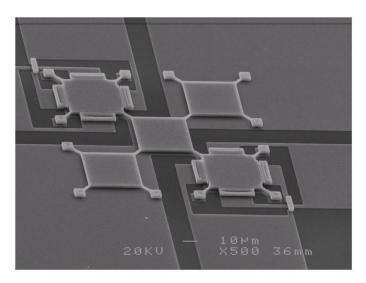
$$Mu'' + Cu' + Ku = P\phi$$
$$y = V^{T}u.$$

Projection basis Q_n with Second Order ARnoldi (SOAR):

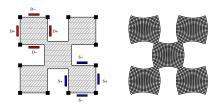
$$M_n u_n'' + C_n u_n' + K_n u_n = P_n \phi$$
$$y = V_n^T u$$

where
$$P_n = Q_n^T P$$
, $V_n = Q_n^T V$, $M_n = Q_n^T M Q_n$, ...

Checkerboard Resonator

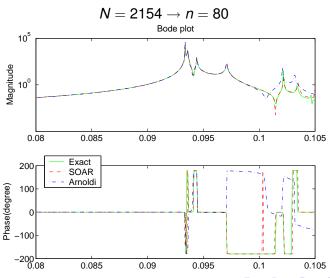


Checkerboard Resonator



- Anchored at outside corners
- Excited at northwest corner
- Sensed at southeast corner
- Surfaces move only a few nanometers

Performance of SOAR vs Arnoldi



Complex Symmetry

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Model with radiation damping (PML) gives complex problem:

$$(K - \omega^2 M)u = f$$
, where $K = K^T, M = M^T$

Forced solution *u* is a stationary point of

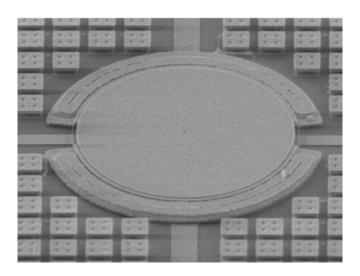
$$I(u) = \frac{1}{2}u^{T}(K - \omega^{2}M)u - u^{T}f.$$

Eigenvalues of (K, M) are stationary points of

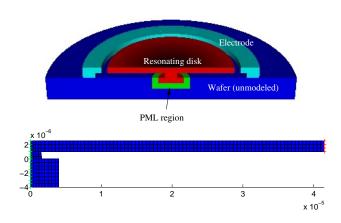
$$\rho(u) = \frac{u^T K u}{u^T M u}$$

First-order accurate vectors ⇒ second-order accurate eigenvalues.

Disk Resonator Simulations



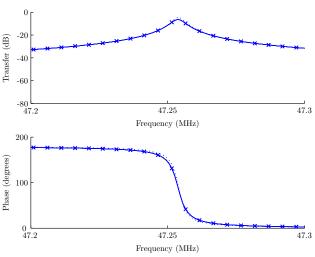
Disk Resonator Mesh



- Axisymmetric model with bicubic mesh
- About 10K nodal points in converged calculation



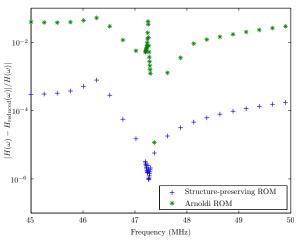
Symmetric ROM Accuracy



Results from ROM (solid and dotted lines) near indistinguishable from full model (crosses)

Symmetric ROM Accuracy

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Preserve structure ⇒ get twice the correct digits



Perturbative Structure

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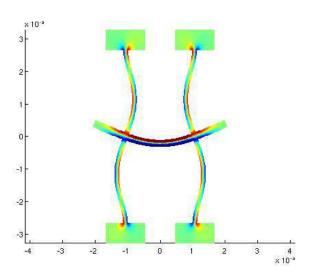
Dimensionless continuum equations for thermoelastic damping:

$$\sigma = \hat{C}\epsilon - \xi\theta\mathbf{1}
\ddot{u} = \nabla \cdot \sigma
\dot{\theta} = \eta \nabla^2 \theta - \operatorname{tr}(\dot{\epsilon})$$

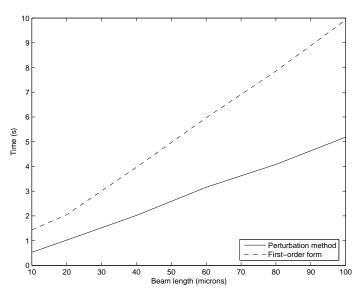
Dimensionless coupling ξ and heat diffusivity η are 10^{-4} \implies perturbation method (about $\xi = 0$).

Large, non-self-adjoint, first-order coupled problem \to Smaller, self-adjoint, mechanical eigenproblem + symmetric linear solve.

Thermoelastic Damping Example



Performance for Beam Example



Aside: Effect of Nondimensionalization

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100 μ m beam example, first-order form.

Before nondimensionalization

• Time: 180 s

• nnz(L) = 11M

After nondimensionalization

• Time: 10 s

• nnz(L) = 380K

Semi-Analytical Model Reduction

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We work with hand-build model reduction all the time!

- Circuit elements: Maxwell equation + field assumptions
- Beam theory: Elasticity + kinematic assumptions
- Axisymmetry: 3D problem + kinematic assumption

Idea: Provide global shapes

- User defines shapes through a callback
- Mesh serves defines a quadrature rule
- Reduced equations fit known abstractions



Global Shape Functions

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Normally:

$$u(X) = \sum_{j} N_{j}(X)\hat{u}_{j}$$

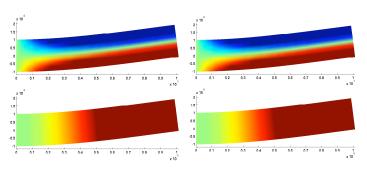
Global shape functions:

$$\hat{u} = \hat{u}^I + G(\hat{u}^g)$$

Then constrain values of some components of \hat{u}^{l} , \hat{u}^{g} .

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Which mode shape comes from the reduced model (3 dof)?



(Left: 28 MHz; Right: 31 MHz)

Conclusions

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Respecting problem structure is a Good Thing!

- ODE structure
- Complex symmetric structure
- Perturbative structure
- Geometric structure

Result:

Better accuracy, faster set-up, better understanding.