

# HiQLab: Simulation of Resonant MEMS

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# Overview

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### The Basics

### Anchor loss

### Thermoelastic damping

### Checkerboard and ROM

### Wrap-up

- Background, target applications, and grand vision
- Simple “from scratch” examples
- Anchor loss in a disk resonator
- Thermoelastic damping in a beam
- Model reduction of a checkerboard resonator
- Current status and planned work
- Q & A and feedback

# Application: RF MEMS

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» Sources of damping

» What makes it hard?

» Goal for HiQLab

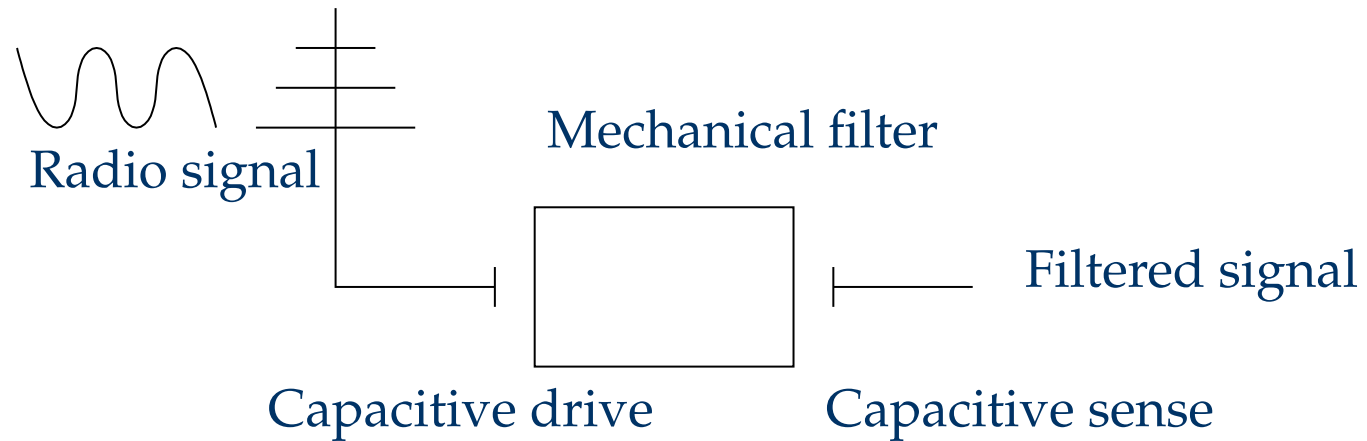
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Wrap-up



- Systems of MHz-GHz mechanical resonators
- Useful for
  - ◆ Frequency references
  - ◆ Filter elements
  - ◆ Sensing elements

# Damping and $Q$

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- Want to minimize damping
  - ◆ Electronic filters have too much
  - ◆ Understanding of damping in MEMS resonators is lacking
- Characterize damping by  $Q$ 
  - ◆ Non-dimensionalized damping in a one-variable system:

$$\frac{d^2u}{dt^2} + Q^{-1} \frac{du}{dt} + u = F(t)$$

- ◆ For a resonant mode with frequency  $\omega \in \mathbb{C}$ :

$$Q := \frac{\Re(\omega)}{2\Im(\omega)} = \frac{\text{Stored energy}}{\text{Energy loss per radian}}$$

- Goal: Make  $Q$  big

# Sources of damping

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- Fluid damping
  - ◆ Air is a viscous fluid ( $Re \ll 1$ )
  - ◆ Can operate in a vacuum
  - ◆ Shown not to dominate in many RF designs
- Anchor loss
  - ◆ Elastic waves radiate from structure
- Thermoelastic damping
  - ◆ Volume changes induce temperature change
  - ◆ Diffusion of heat leads to mechanical loss
- Material losses (catch-all)
  - ◆ Low intrinsic losses in silicon, diamond, germanium, etc.
  - ◆ Greater material losses in metals

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- Physical issues
  - ◆ Not clear which loss mechanisms dominate
  - ◆ Need physically realistic models
  - ◆ Need good material property estimates
- Mathematical issues
  - ◆ Operating modes are in the middle of the spectrum
  - ◆ Damping makes the problem naturally nonsymmetric
  - ◆  $\omega$  must be accurately resolved to estimate  $Q$
  - ◆ Symmetries and near-symmetries lead to degeneracy
  - ◆ Dependence on parameters is critical

# Goal for HiQLab

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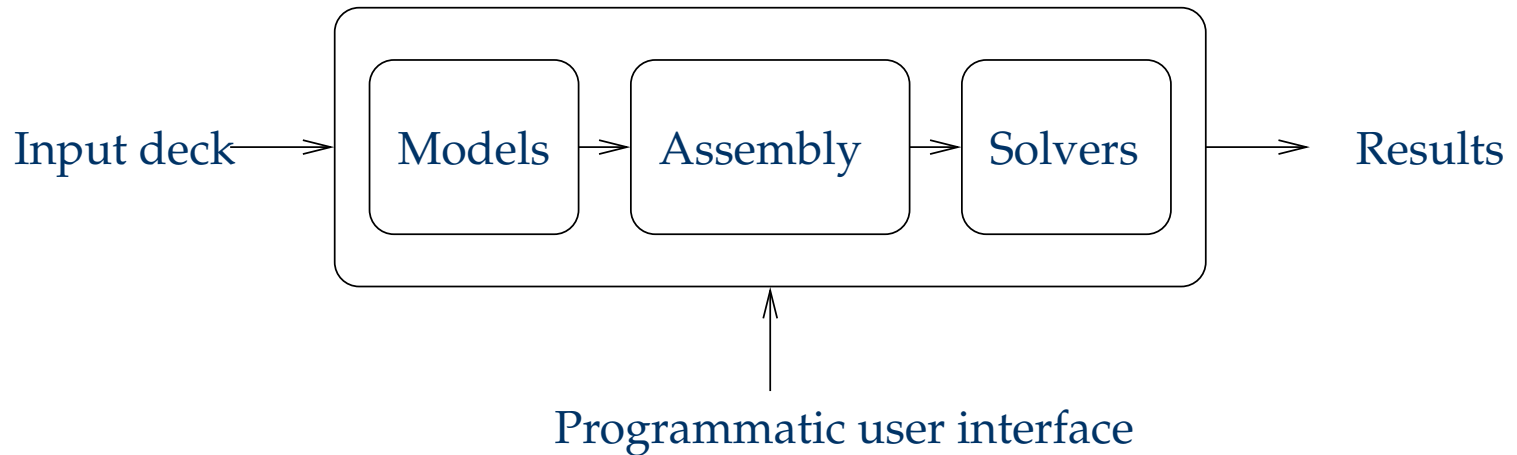
Thermoelastic damping

Checkerboard and ROM

Wrap-up

- Goal is to understand resonant MEMS behavior
  - ◆ Initially targeting high-frequency MEMS
  - ◆ Particularly care about damping
  - ◆ Want to experimentally verify our simulations
- Reason for the simulator
  - ◆ Develop physically realistic models
  - ◆ Develop fast solvers
  - ◆ Help designers

# Software structure



- Element models (C++)
- Mesh management and system assembly (C++)
- Solvers
  - ◆ Standard low-level solver libraries (Fortran, C/C++)
  - ◆ High-level solvers provided by MATLAB
  - ◆ Specialized algorithms in MATLAB or C++
- Mesh description (Lua)
- User interfaces (MATLAB, Lua)

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# Software used

“Lesser artists borrow. Great artists steal.”  
– Picasso, Dali, Stravinsky?

- Lua: [www.lua.org](http://www.lua.org)
  - ◆ Evolved from simulator data languages (DEL and SOL)
  - ◆ Pascal-like syntax fits on one page; complete language description is 21 pages
  - ◆ Fast, freely available, widely used in game design
- MATLAB: [www.mathworks.com](http://www.mathworks.com)
  - ◆ “The Language of Technical Computing”
  - ◆ Good sparse matrix support
  - ◆ Star-P: <http://www.interactivesupercomputing.com/>
- Standard numerical libraries: ARPACK, UMFPACK

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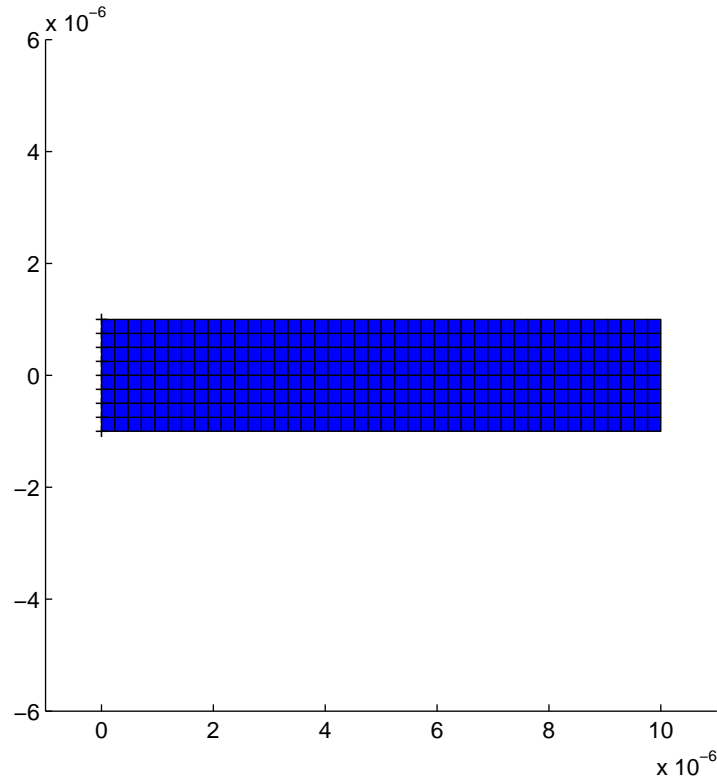
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- Describe a simple cantilever
- Compute and plot the modes of vibration
- Perform a parameter study

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```
require './common.lua'
```

```
l = 10e-6           -- Beam length
w = 2e-6            -- Beam width
dense = 0.5e-6      -- Approximate element size
order = 2           -- Order of elements
nen = 9             -- Number of element nodes
```

- Common header file defines materials, block generator
- Define symbols for geometry and meshing parameters
- “-” indicates the start of a comment

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```
mesh = Mesh:new(2, nen, 2)
mat   = make_material('silicon2', 'planestrain',
                    order)
blocks( { 0, 1 }, { -w/2.0, w/2.0 }, mat )
```

- Define a new mesh (which *must* be called mesh)
  - ◆ Number of dimensions = 2
  - ◆ Number of element nodes = nen
  - ◆ Number of unknowns per node = 2
- Define a polysilicon material in plane strain
- Mesh the region  $[0, l] \times [-w/2, w/2]$ 
  - ◆ Element size  $h$  is determined by dense

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```
mesh:set_bc(function(x,y)
    if x == 0 then return 'uu', 0, 0; end
end)
```

- Define boundary conditions with a function evaluated at every node
- Function returns
  - ◆ A string to specify displacement or force BCs
  - ◆ Values of boundary displacements or forces
- Examples:
  - ◆ Returns nothing – no boundary conditions
  - ◆ 'uu', 0, 0 – zero displacement in both  $x$  and  $y$
  - ◆ 'u', 0 – zero displacement in  $y$  only
  - ◆ 'f', 1 – unit force in the  $x$  direction
  - ◆ 'uf', 0, 1 – zero  $x$  displacement, unit force in  $y$

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Wrap-up

```
>> run ../../init.m
```

```
HiQlab 0.1
```

```
Copyright      : Regents of the University of California
```

```
Build system:  i686-pc-linux-gnu
```

```
Build date   : Wed Dec 15 12:50:48 PST 2004
```

```
Bug reports  : dbindel@cs.berkeley.edu
```

- In MATLAB, you *must* run init first
- If you don't see the banner, there is a problem

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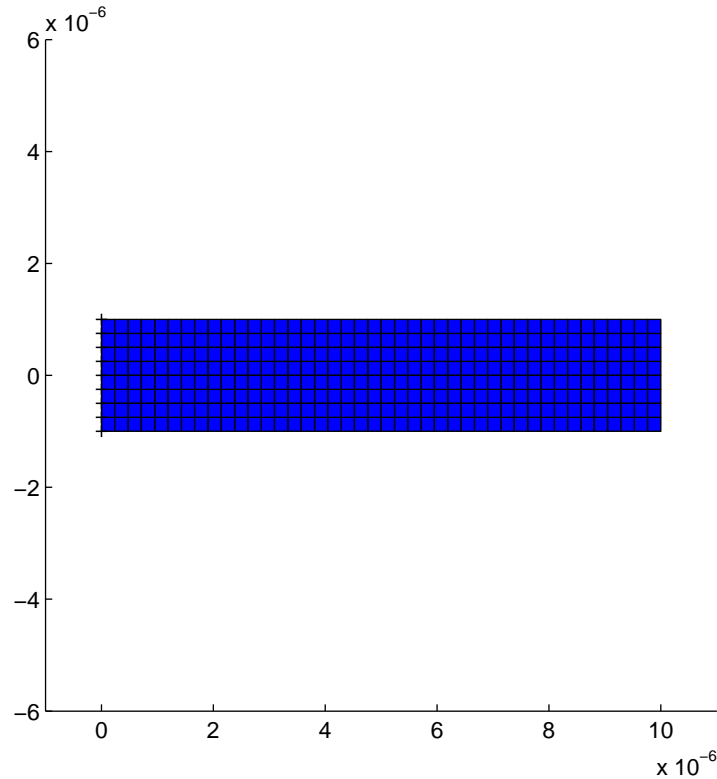
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```
>> mesh = Mesh_load('beammesh.lua');  
>> plotmesh(mesh); axis equal
```

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$$(K - \omega^2 M)v = 0$$

```
>> [M,K] = Mesh_assemble_mk(mesh);  
>> [V,D] = eigs(K,M, 5, 'sm');  
>> w = sqrt(diag(D))/2/pi;
```

```
W =  
1.0e+08 *  
0.2791 + 0.0000i  
1.4947 - 0.0000i  
2.2295 - 0.0000i  
3.5475 - 0.0000i  
5.8811 - 0.0000i
```



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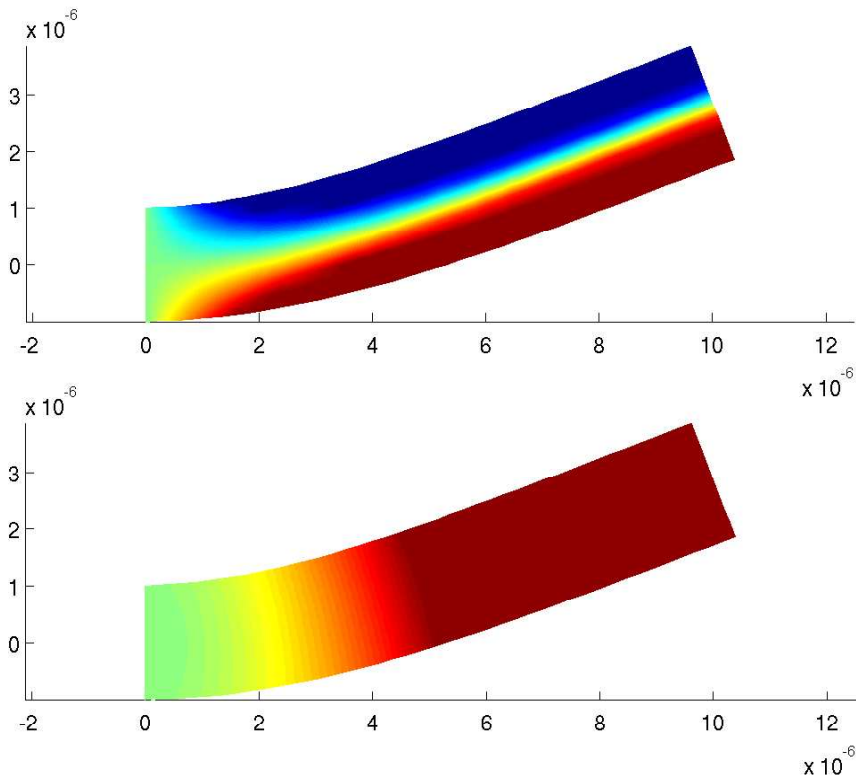
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Wrap-up



```
>> opt.axequal = 1;  
>> opt.deform = 1;  
>> Mesh_scale_u(mesh, V(:,1), 2, 1e-6);  
>> plotfield2d(mesh, opt)
```

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Change one line in Lua file:

```
l = 1 or 10e-6      -- Beam length
```

Now set `l` from MATLAB:

```
l = linspace(10e-6, 20e-6, 11);
for k = 1:length(l)
    param.l = l(k);
    mesh = Mesh_load('beammesh2.lua', param);
    [M,K] = Mesh_assemble_mk(mesh);
    w(k) = sqrt(eigs(K,M,1, 'sm'))/2/pi;
    Mesh_delete(mesh);
end
plot(l,real(w)); axis tight
```

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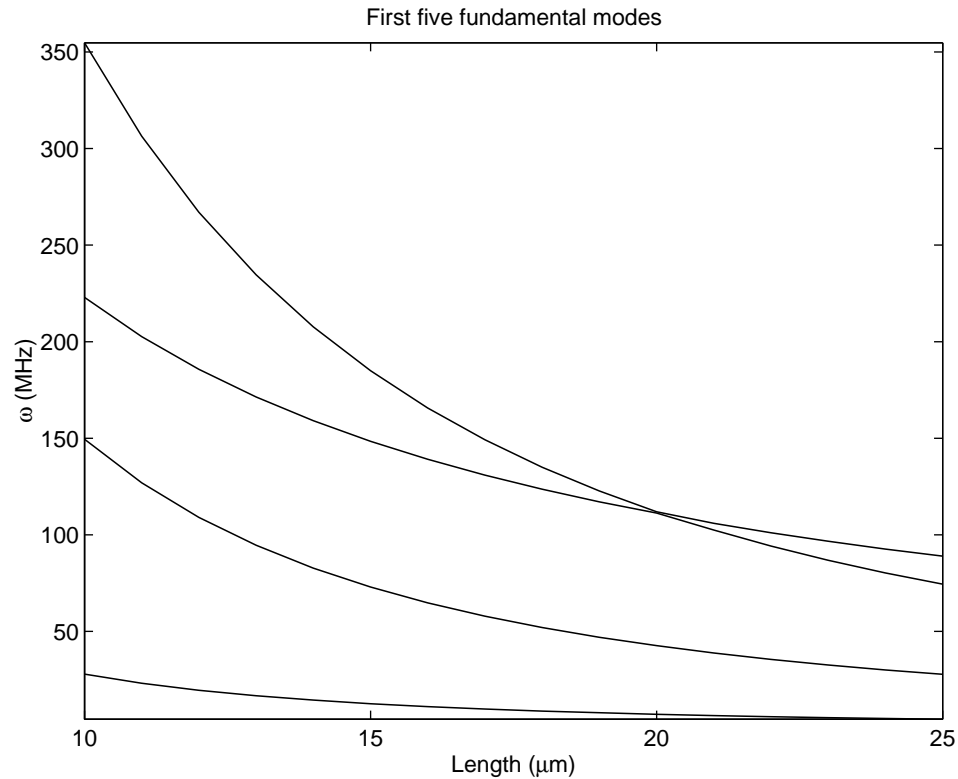
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- Change two lines to plot *several* frequencies
- Notice crossing behavior of third and fourth modes

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```
[tutorial]: hiqlab driver.lua
1          :          27.908006867444 MHz
2          :          149.46698798698 MHz
3          :          222.95156567429 MHz
4          :          354.75135363746 MHz
5          :          588.11440349498 MHz
```

- Can run simulations in standalone code
- Missing some capabilities (esp graphics)
- Less overhead than MATLAB interface

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```
beamf = loadfile 'beammesh.lua'

w0    = 0    -- Frequency estimate
nev   = 5    -- Number of eigs
ncv   = 10   -- Size of space (~2 nev)
dr    = {}   -- Real parts of eigs
di    = {}   -- Imag parts of eigs

-- Load mesh and compute eigs
beamf()
mesh:initialize()
compute_eigs(mesh, w0, nev, ncv, dr, di);

-- Print eigs
for k = 1,5 do
    print(k, ':', dr[k]/2e6/pi, 'MHz')
end
```

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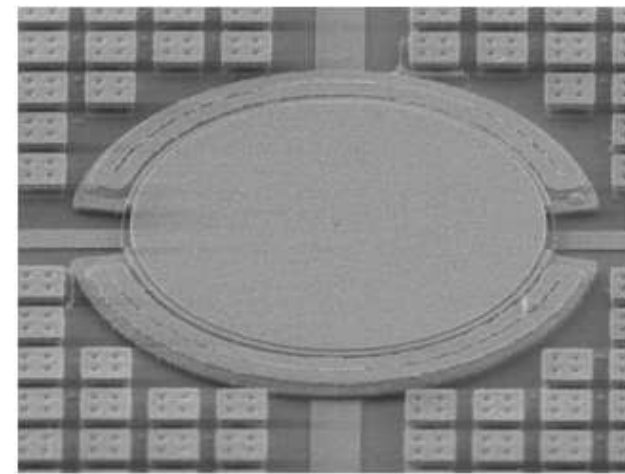
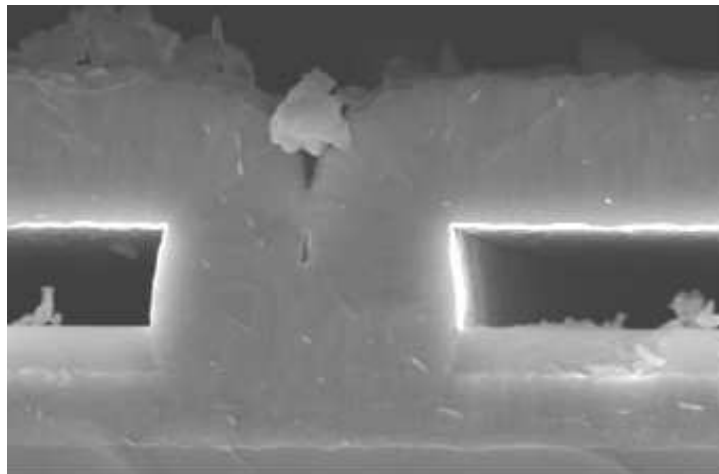
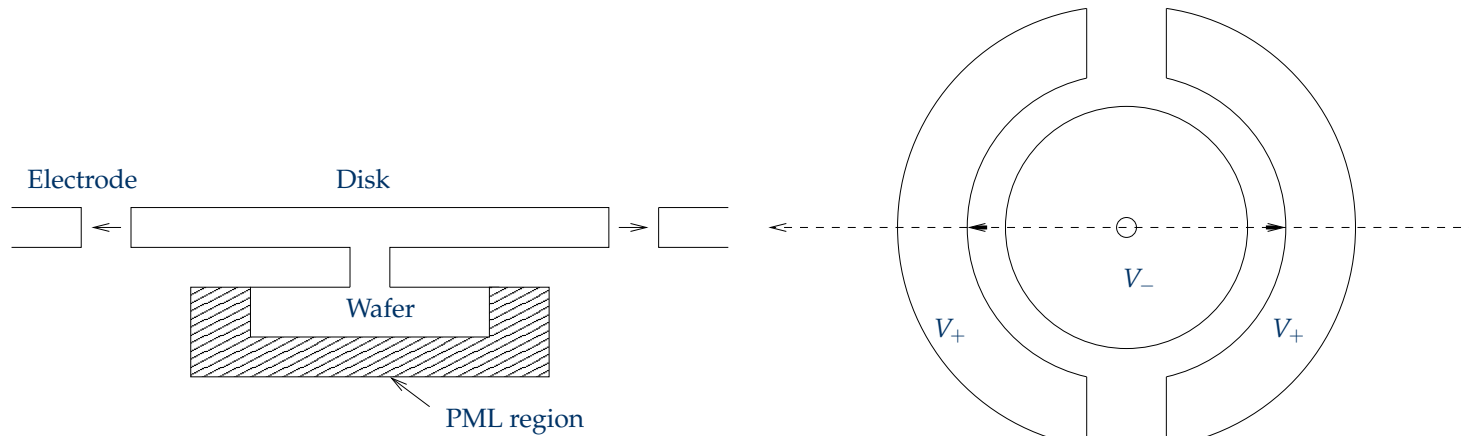
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- SiGe disk resonators built by E. Quévy
- Axisymmetric model with bicubic mesh, about 10K nodal points

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Goal: Understand energy loss in this resonator

- Dominant loss is elastic radiation from anchor.
- Disk resonator is much smaller than substrate
- Very little energy leaving the post is reflected back
  - ◆ Substrate is semi-infinite from disk's perspective
- Possible semi-infinite models
  - ◆ Matched asymptotic modes
  - ◆ Dirichlet-to-Neumann maps
  - ◆ Boundary dampers
  - ◆ Perfectly matched layers

# Perfectly matched layers

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- Apply a complex coordinate transformation
- Generates a non-physical absorbing layer
- No impedance mismatch between the computational domain and the absorbing layer
- Idea works with general linear wave equations
  - ◆ First applied to Maxwell's equations (Bereng er 95)
  - ◆ Similar idea introduced earlier in quantum mechanics (*exterior complex scaling*, Simon 79)



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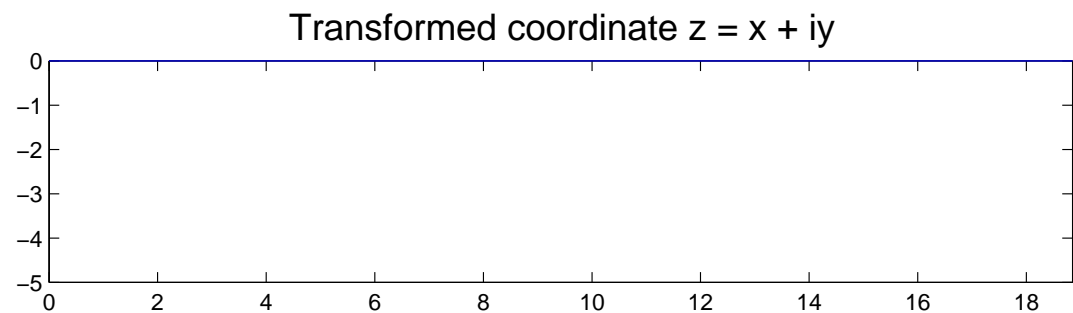
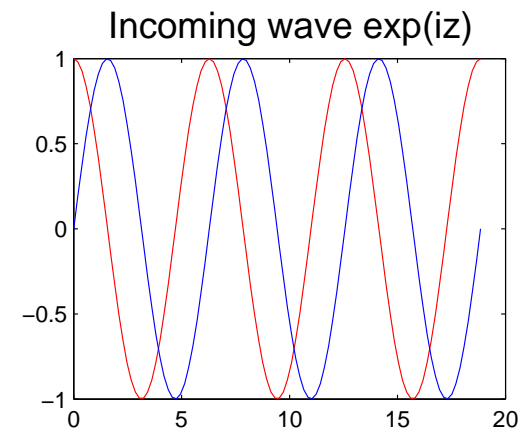
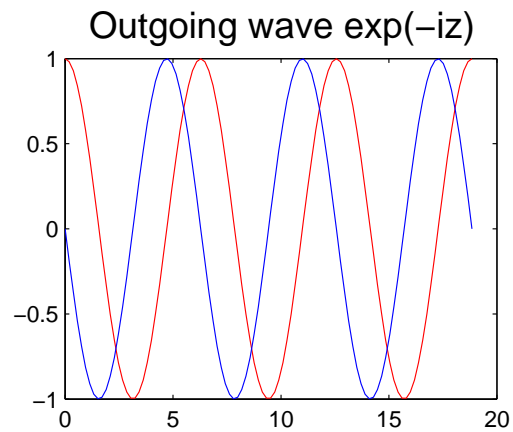
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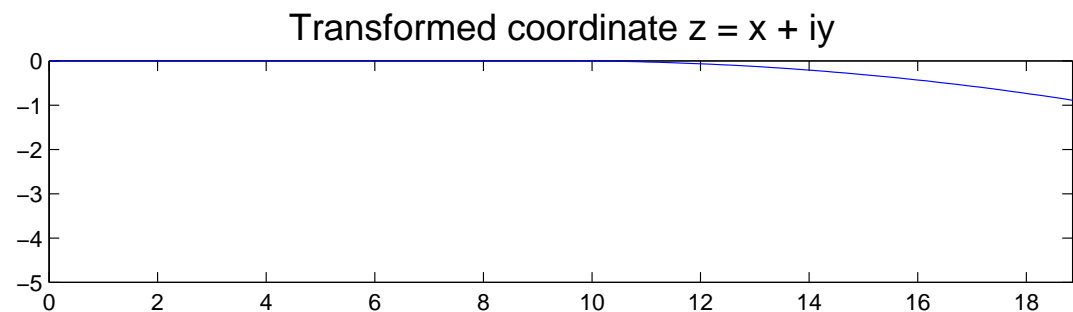
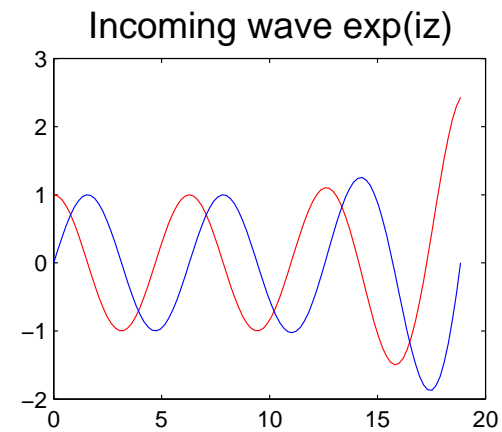
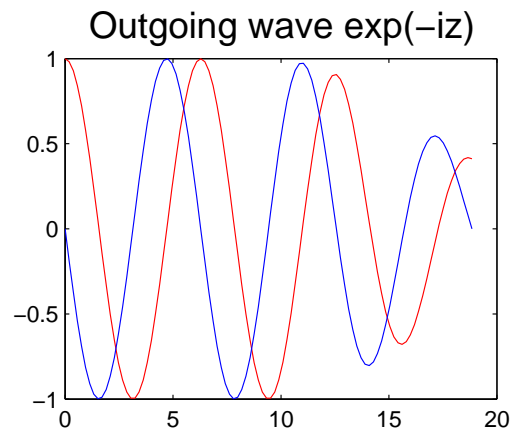
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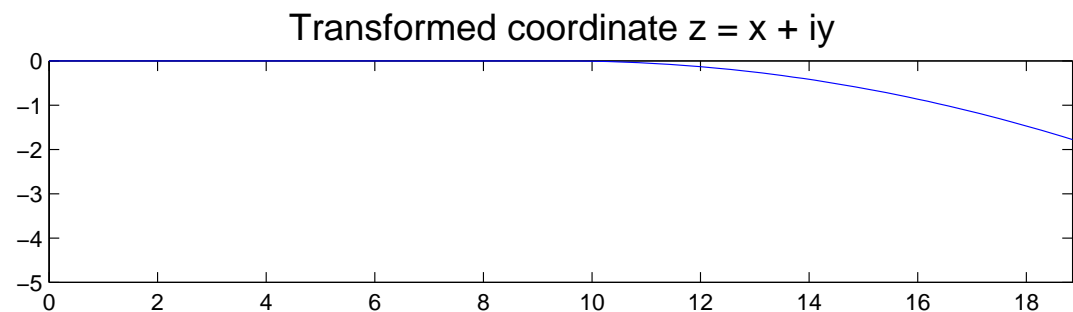
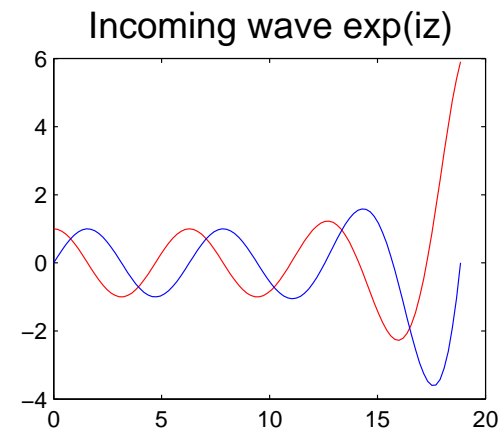
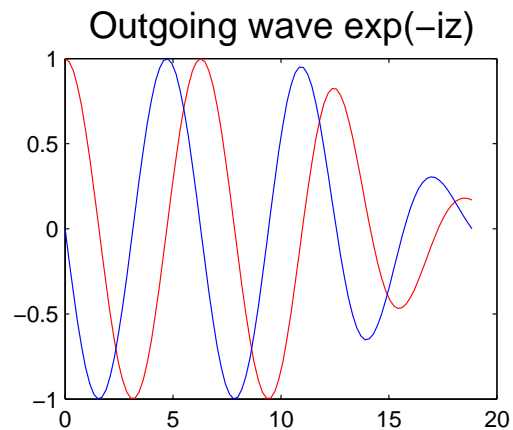
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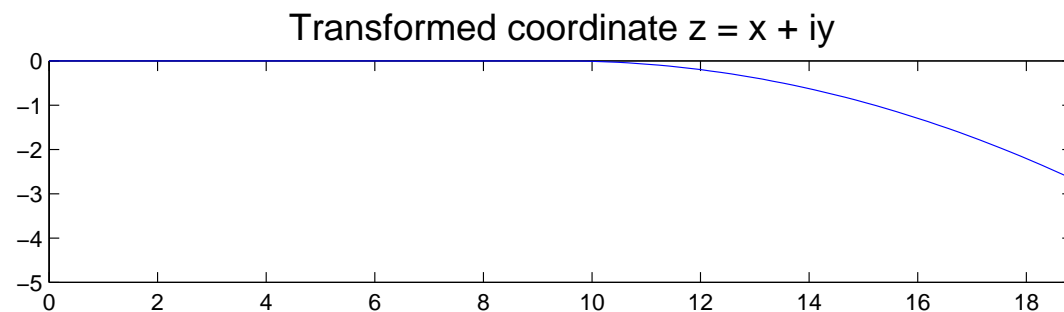
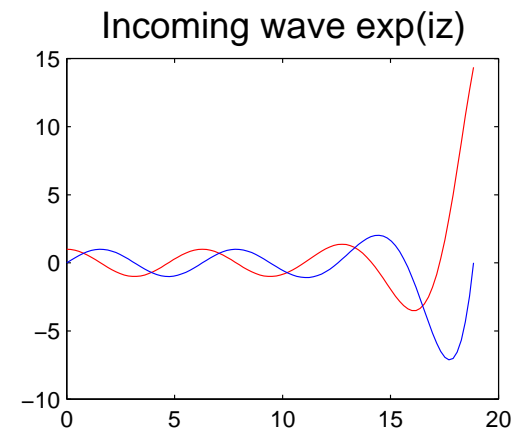
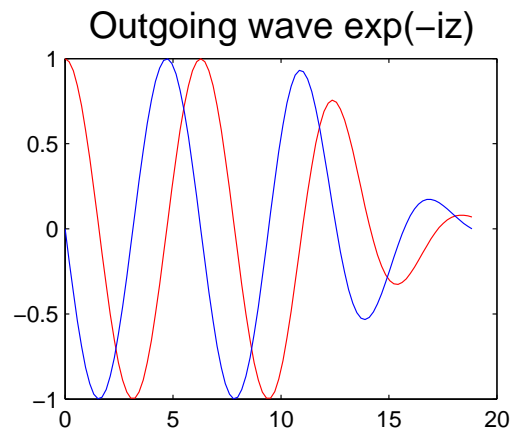
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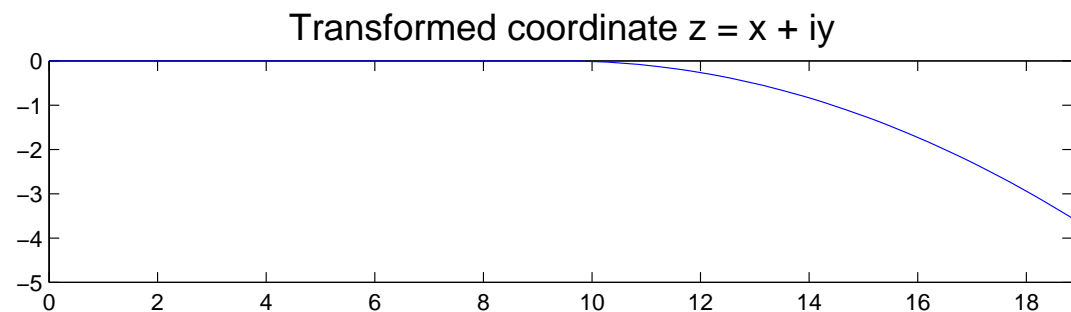
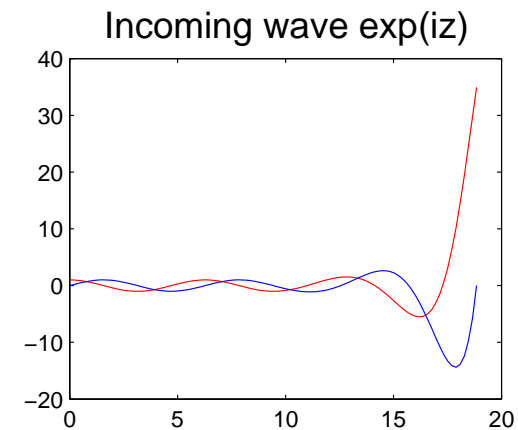
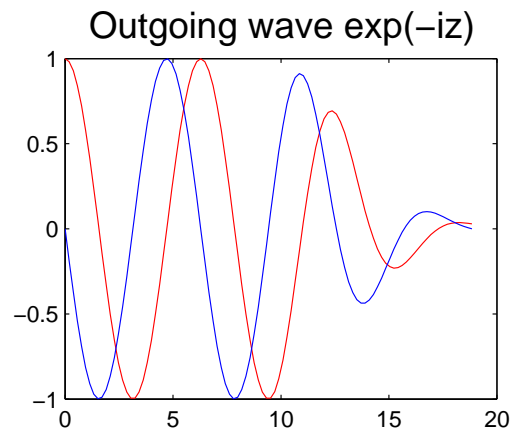
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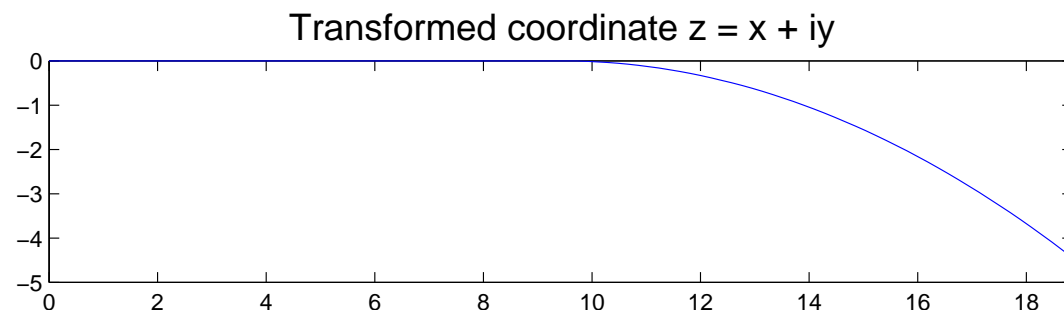
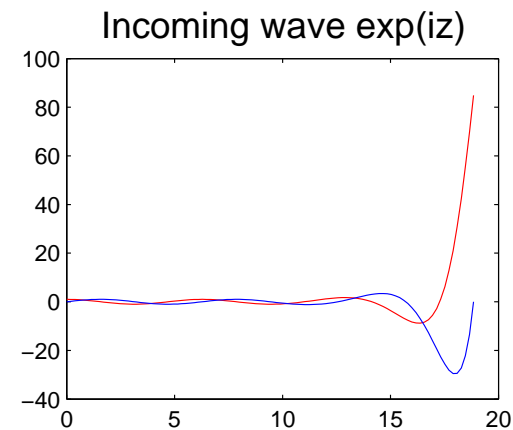
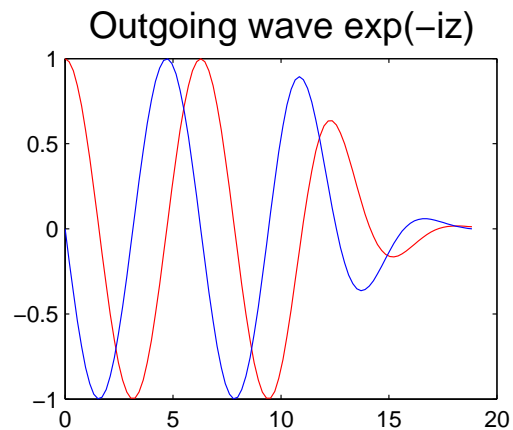
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Wrap-up



Clamp solution at transformed end to isolate outgoing wave.

# Defining the PML

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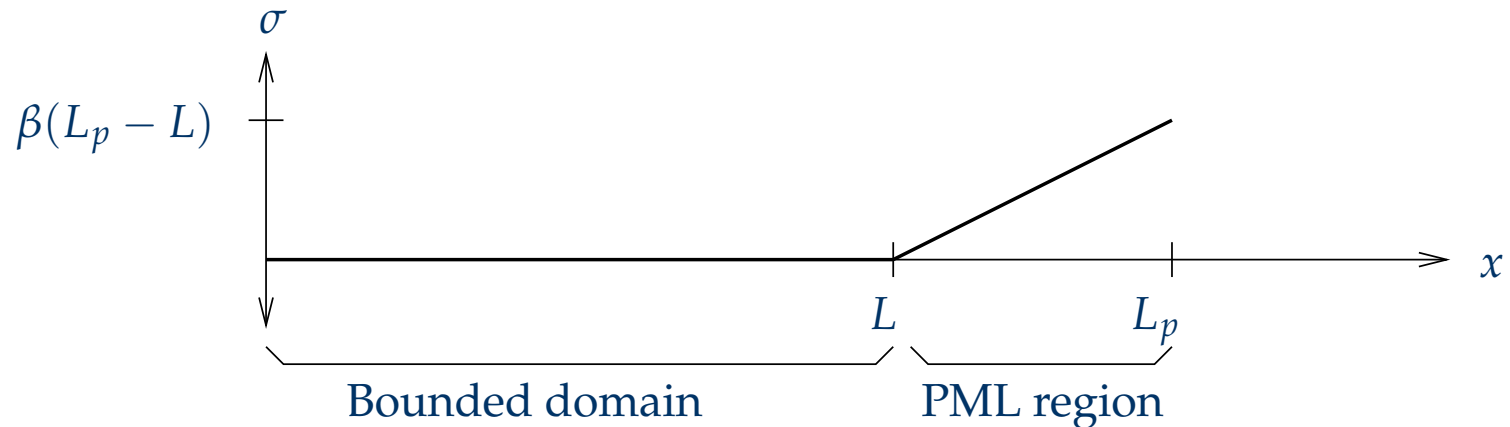
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- Only need  $dz/dx = 1 - i\sigma(x)$
- Usually choose  $\sigma$  to be piecewise linear
  - ◆  $\sigma = 0$  on ordinary domain
  - ◆  $\sigma > 0$  in PML region
- In higher dim, transform each  $x_i$  independently

# Scalar wave in HiQLab

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Wrap-up

```
require './common.lua'
```

```
Ne1 = Ne1 or 10 -- Elements in first region  
Ne2 = Ne2 or 10 -- Elements in second region  
order = order or 3 -- Polynomial order  
nen = order+1; -- Number of element nodes
```

```
mesh = Mesh:new(1, nen, 1);  
D = mesh:own( PMLScalar1d:new(1, 1, nen) );  
mesh:add_block(-Ne1, Ne2, order*(Ne1+Ne2)+1,  
              D, order);
```

- Mesh  $[-N_1, N_2]$  with cubic elements
- Define a material for a scalar wave with PML



# Scalar wave BCs

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Wrap-up

```
epw = epw or 10 -- Elements per wave
dpw = dpw or 1  -- Damping per wave
```

```
D:set_stretch(function(x)
    return max(x*dpw/epw, 0)
end)
```

```
mesh:set_bc(function(x)
    if x == -Nel then return 'u', 1 end
end)
```

- $\sigma(x) = 0$  on  $[-N_1, 0]$
- $\sigma(x)$  varies linearly from 0 to 1 on  $[0, N_2]$ 
  - ◆  $\sigma_{\max}$  small only for demonstration
  - ◆ A more reasonable  $\sigma_{\max}$  would be 10 – 40
- Displacement BCs at left end generate waves

# MATLAB driver

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```
mesh = Mesh_load('pml1d.lua');  
k = 2*pi/10;  
Mesh_make_harmonic(mesh, k);  
[M,K] = Mesh_assemble_mk(mesh);  
F = Mesh_assemble_R(mesh);  
u = -(K-k^2*M)\F;  
Mesh_set_u(mesh, u);
```

- `Mesh_make_harmonic` sets  $v = i\omega u$  and  $a = -\omega^2 u$
- $F$  is the forcing vector from BCs
- $u$  is the time-harmonic response

# MATLAB driver

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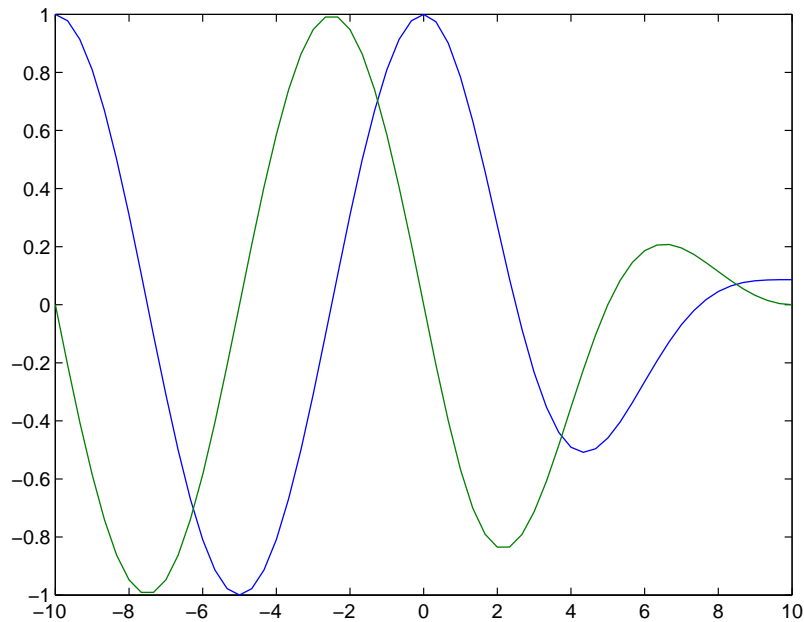
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```
x = Mesh_get_x(mesh);  
u = Mesh_get_disp(mesh);  
plot(x, real(u), x, imag(u));  
Mesh_delete(mesh);
```

# Disk mesh

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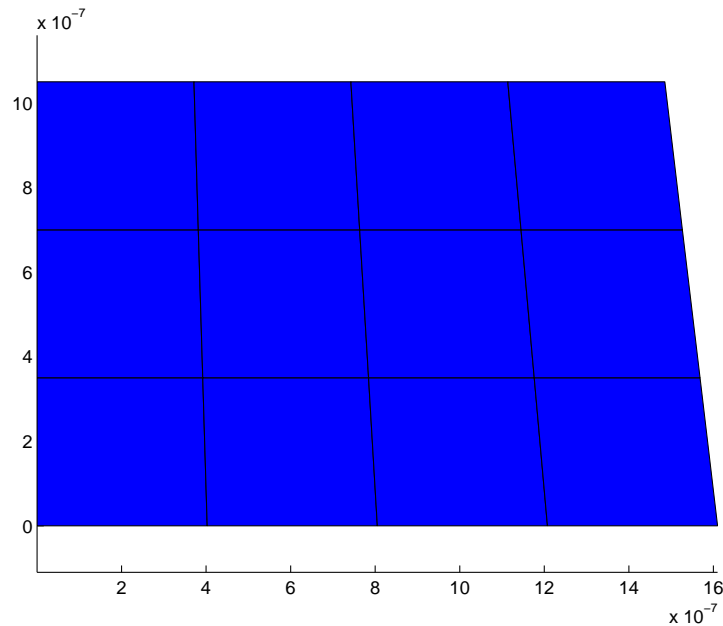
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```
mesh:add_block_shape(npostx, ndisky, pelt, order,  
                    {0,      0,      0,      hpost,  
                     rpost2, 0,      rpost, hpost})
```

Mesh of mapped blocks. Arguments specify block size, type of element, and  $(x, y)$  coordinates of each corner.

# Disk mesh

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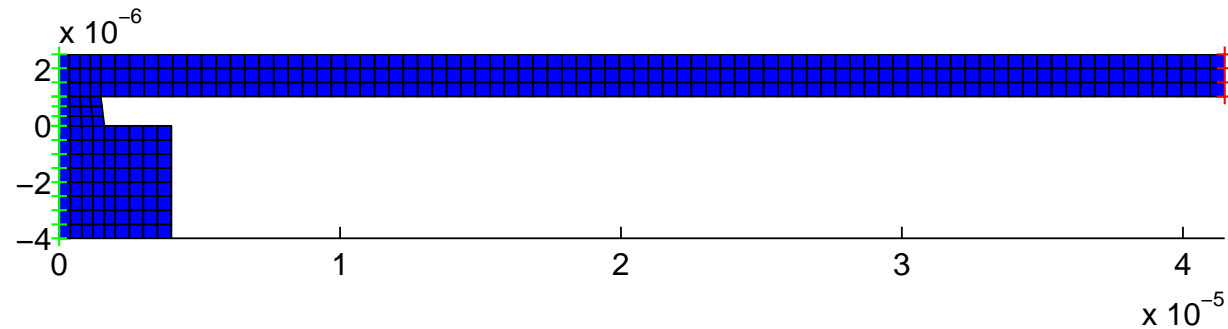
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```
mesh:tie(dense/100)
```

Mapped blocks are tied together to form disk mesh.  
Usually use higher mesh density than shown.

# Forced response

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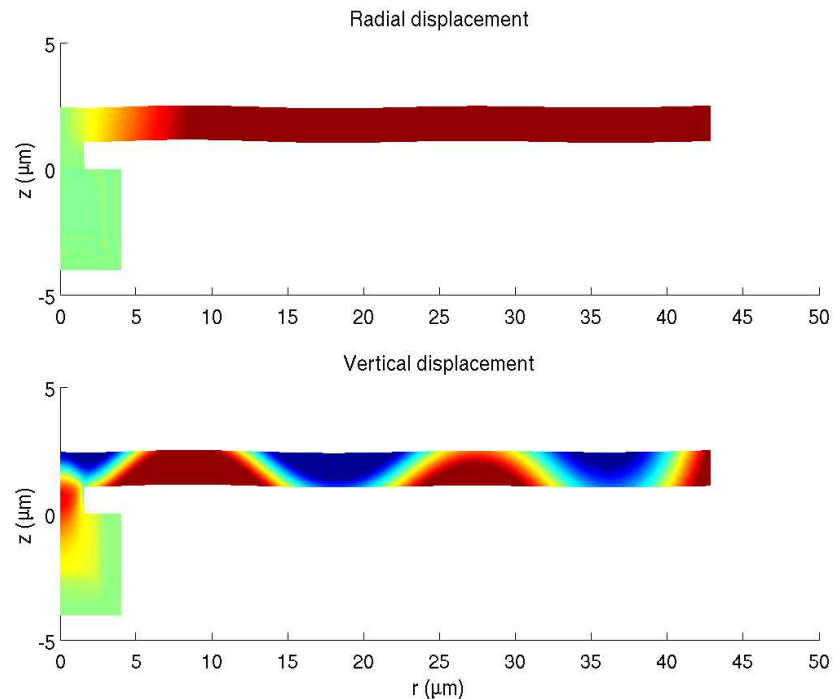
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Wrap-up



```
mesh = Mesh_load('diskmesh.lua', param);  
[M,K] = Mesh_assemble_mk(mesh);  
F      = Mesh_assemble_R(mesh);  
u      = -(K - wforce^2*M) \ F;  
Mesh_scale_u(mesh, u, 1, 1e-6);  
plotcycle2d(mesh,1,plotopt);
```

# Time-averaged energy flux

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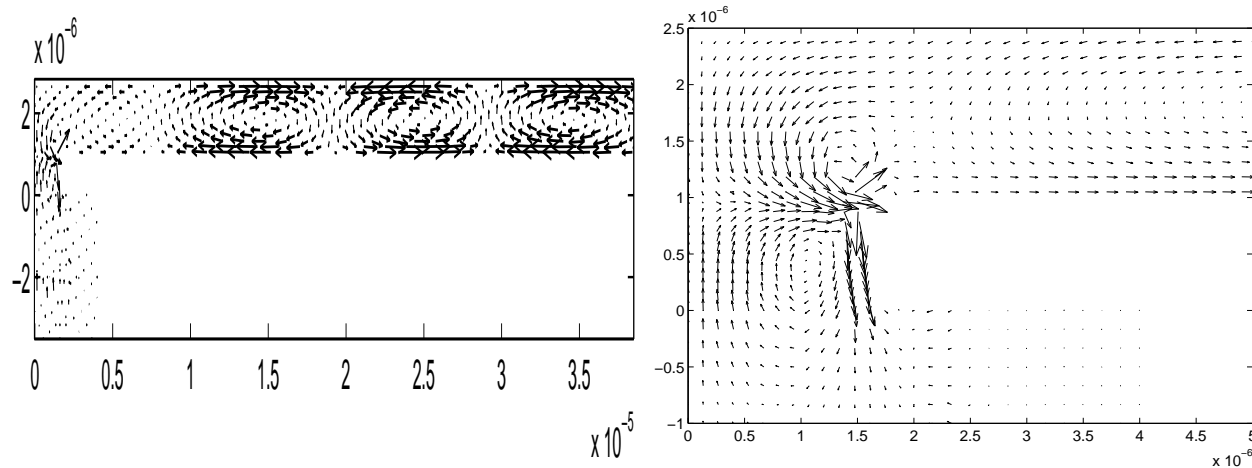
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```
Mesh_make_harmonic(mesh, wforce);  
p = Mesh_get_x(mesh);  
E = Mesh_mean_power(mesh);  
quiver(p(1,:), p(2,:), E(1,:), E(2,:));
```

- Compute  $\bar{E} = T^{-1} \int_0^T \sigma(t) \cdot v(t) dt$
- Energy flows are strongest at surfaces
- Stress singularity at corner sprays energy

# Damped modes

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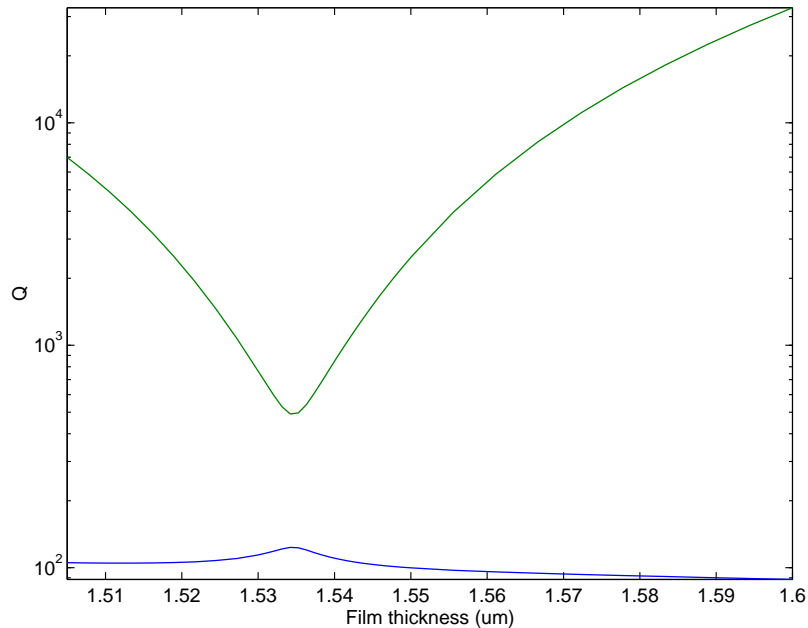
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In a loop, compute

```
param.hdisk = t(k);  
mesh = Mesh_load('diskmesh.lua', param);  
[M,K] = Mesh_assemble_mk(mesh);  
[VV,w,Q] = pml_mode(M,K,w0,2);  
Mesh_delete(mesh);
```



# Q variation

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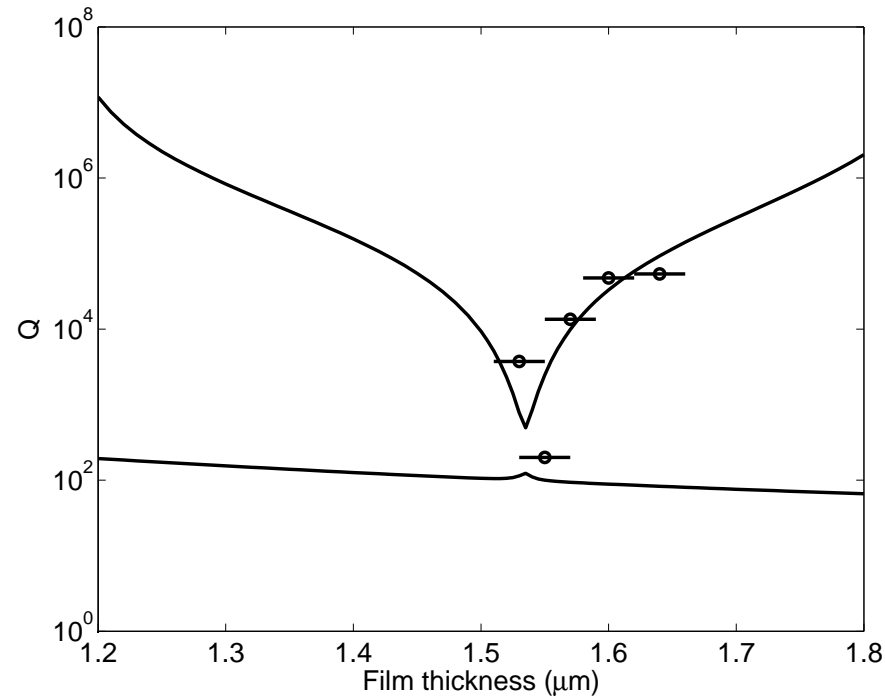
» Q variation

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- Surprising variation in  $Q$  as film thickness changes
- Confirmed by experiment on a set of  $40 \mu\text{m}$  disks
- Effect comes from interaction of radial and bending modes

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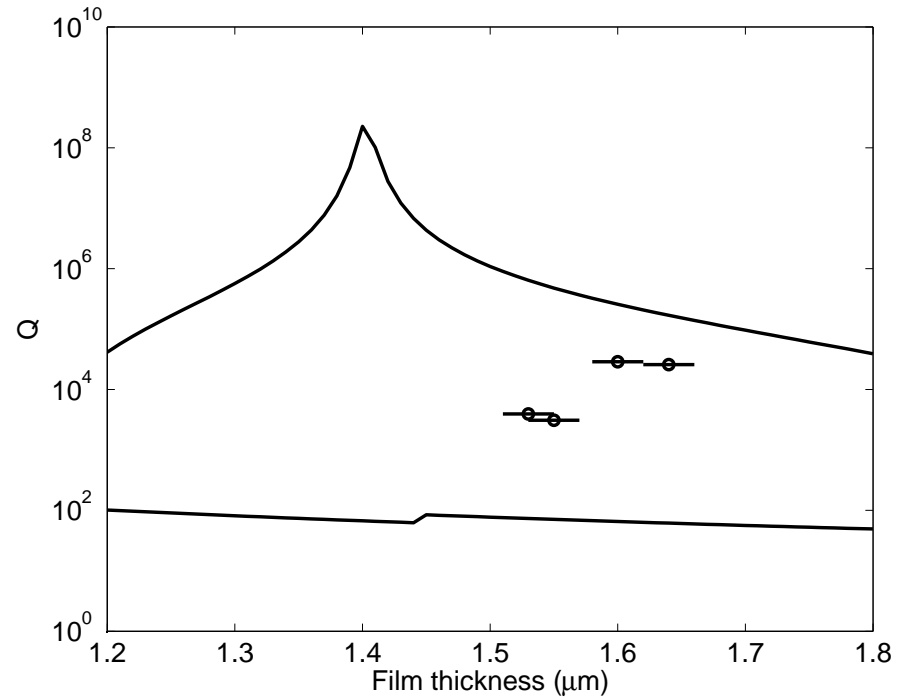
» Q variation

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Wrap-up



Data from a set of  $30\mu\text{m}$  radius disks.

# Thermoelastic damping (TED)

$u$  is displacement and  $T = T_0 + \theta$  is temperature

$$\sigma = C\epsilon - \beta\theta \mathbf{1}$$

$$\rho u_{tt} = \nabla \cdot \sigma$$

$$\rho c_v \theta_t = \nabla \cdot (\kappa \nabla \theta) - \beta T_0 \text{tr}(\epsilon_t)$$

- Volumetric strain rate drives energy transfer from mechanical to thermal domain
  - ◆ Irreversible diffusion  $\implies$  mechanical damping
  - ◆ Not often an important factor at the macro scale
  - ◆ Recognized source of damping in microresonators
- Zener: semi-analytical approximation for TED in beams
- We consider the fully coupled system

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$$\begin{aligned}\sigma &= \hat{C}\epsilon - \tilde{\zeta}\theta\mathbf{1} \\ u_{tt} &= \nabla \cdot \sigma \\ \theta_t &= \eta \nabla^2 \theta - \text{tr}(\epsilon_t)\end{aligned}$$

$$\tilde{\zeta} := \left(\frac{\beta}{\rho c}\right)^2 \frac{T_0}{c_v} \text{ and } \eta := \frac{\kappa}{\rho c_v c L}$$

$$\text{Length} \sim L$$

$$\text{Time} \sim L/c, \text{ where } c = \sqrt{E/\rho}$$

$$\text{Temperature} \sim T_0 \frac{\beta}{\rho c_v}$$

# Scaling analysis

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$$\begin{aligned}\sigma &= \hat{C}\epsilon - \tilde{\zeta}\theta\mathbf{1} \\ u_{tt} &= \nabla \cdot \sigma \\ \theta_t &= \eta \nabla^2 \theta - \text{tr}(\epsilon_t)\end{aligned}$$

$$\tilde{\zeta} := \left(\frac{\beta}{\rho c}\right)^2 \frac{T_0}{c_v} \quad \text{and} \quad \eta := \frac{\kappa}{\rho c_v c L}$$

- Micron-scale poly-Si devices:  $\tilde{\zeta}$  and  $\eta$  are  $\sim 10^{-4}$ .
- Small  $\eta$  leads to thermal boundary layers
- Can linearize about  $\tilde{\zeta} = 0$  for a fast solver
- *Must* note scaling behavior to get accurate eigenvalues

# Clamped SCS beam

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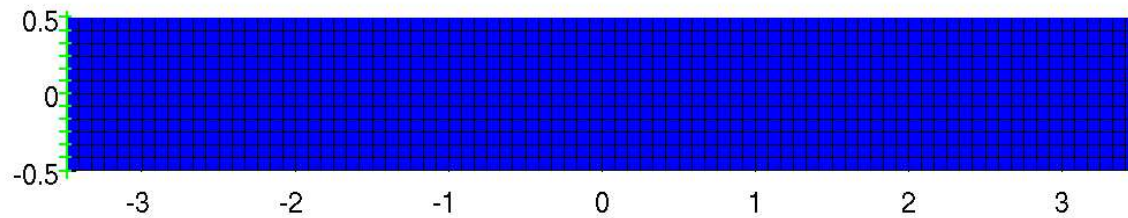
» Scaling analysis

» **Clamped SCS beam**

» Clamped SCS vibration

Checkerboard and ROM

Wrap-up



- Mesh similar to before, but clamped at both ends
- Use full thermoelastic element (single-crystal Si)
- Given length scale and material properties, automatically compute other characteristic scales
- Compute with dimensionless model

# Clamped SCS vibration

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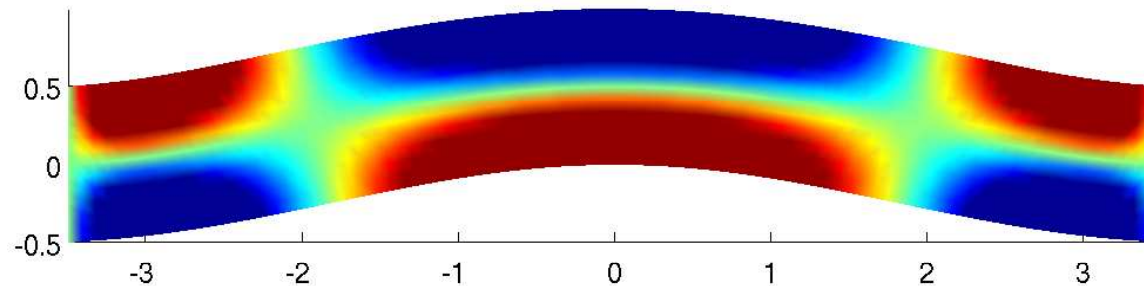
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Wrap-up



$Q = 8700$  at 87.7 MHz

```
tedopt.type = 'pert';  
tedopt.cT   = cT;  
[V,w,Q]    = tedmode(mesh,w0,1,tedopt);
```

- Compute thermoelastic modes using `tedmode`
- Two methods: full solve and perturbation-based
  - ◆ Full solve (default) is more expensive
  - ◆ Perturbation method only works for  $\zeta$  small

# Checkerboard resonator

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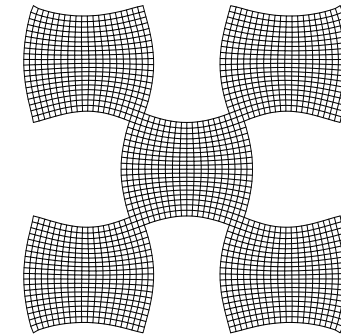
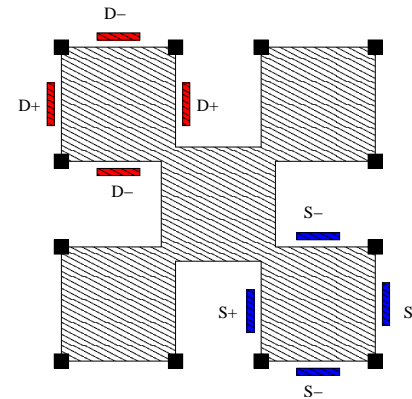
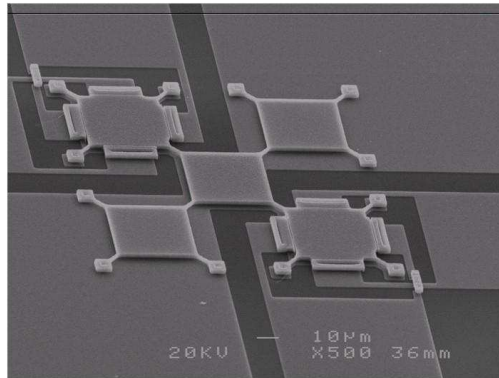
» Checkerboard mesh

» Model reduction

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» Interactive visualization

Wrap-up



- Array of loosely coupled resonators
- Anchored at outside corners
- Excited at **northwest** corner
- Sensed at **southeast** corner
- Surfaces move only a few nanometers



# Checkerboard mesh

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Wrap-up

- A more complex tied mesh example
- Hierarchical: “checker” and “beam” functions
- Can vary
  - ◆ Dimensions
  - ◆ Number of checkers
  - ◆ Linking strategy (corner-coupled or beam-coupled)
  - ◆ Drive and sense positions
- Define functions for drive and sense
  - ◆ Lua functions look like those passed to `set_bc`

```
function drive_checker(x,y)
    ... return string and values ...
end
```
  - ◆ MATLAB functions construct corresponding vectors

```
L = Mesh_get_sense_u(mesh, 'sense_checker');
B = Mesh_get_sense_f(mesh, 'drive_checker');
```

# Model reduction

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Wrap-up

Approximate frequency response near  $\omega_0$  with a  $k$ -dimensional reduced model.

$$H(\omega) = L^T (K - \omega^2 M) B \approx L_k^T (K_k - \omega^2 M_k) B_k$$

```
freq = linspace(wmin, wmax, n);  
[Mk, Kk, Lk, Bk, Vk] = rom_arnoldi(M, K, L, B, k, w0);  
H = compute_bode_mech(freq, Mk, Kk, Lk, Bk);  
plot_bode(freq, H);
```

# Bode plot

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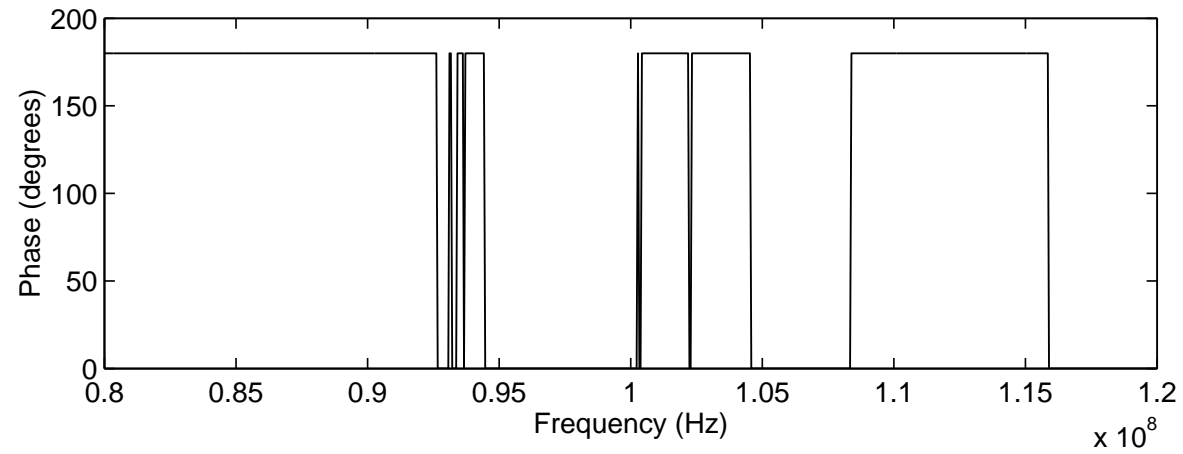
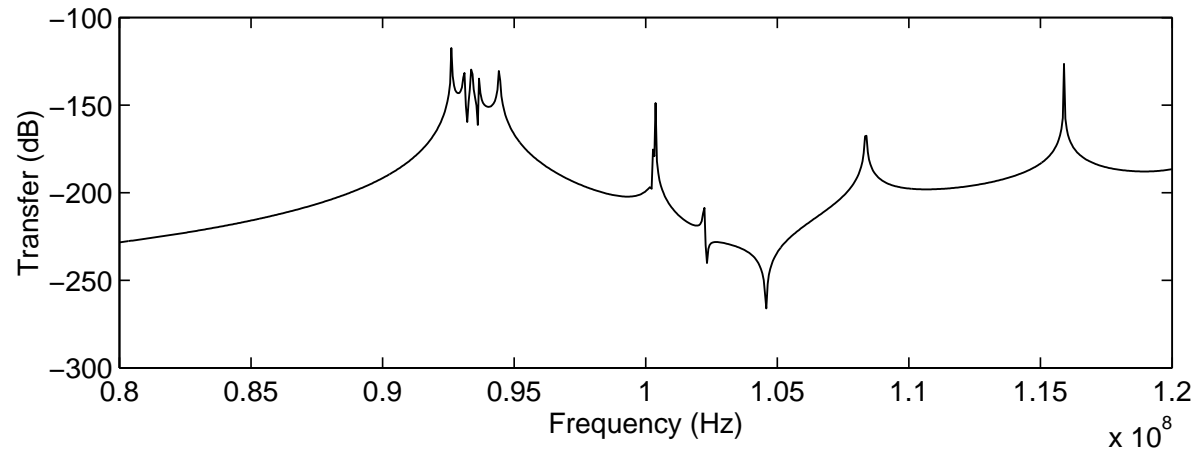
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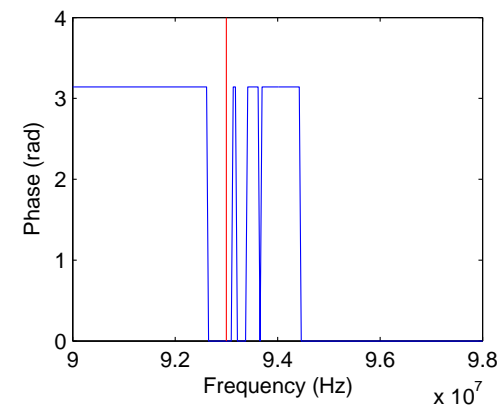
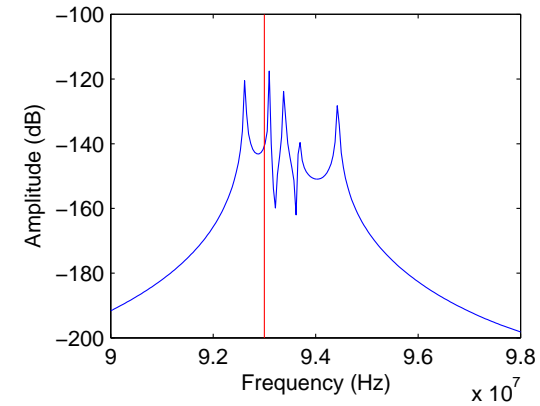
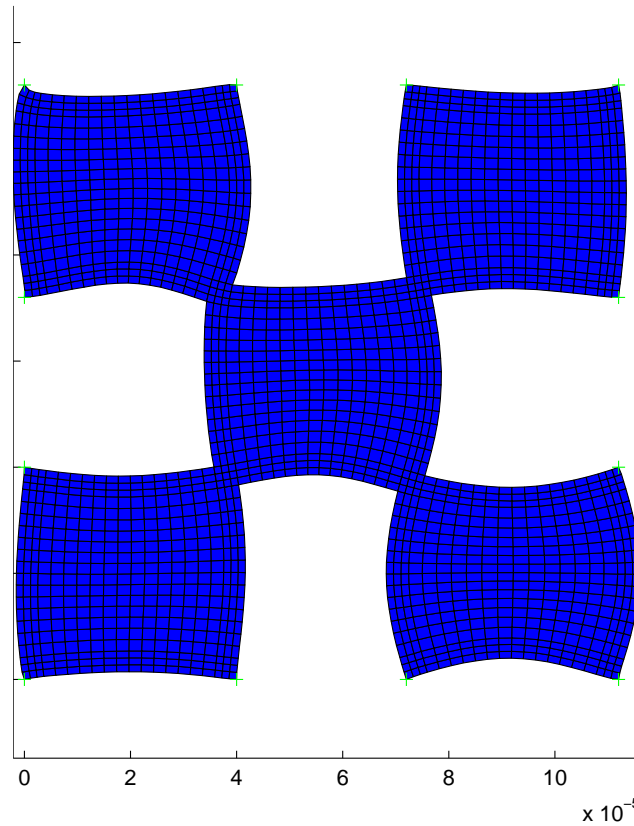
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# Current status

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» Planned work

» Conclusions

- Alpha version available with MATLAB and Lua front-ends
  - ◆ Already allows some interesting analyses
  - ◆ Ongoing verification work (E. Quévy)
- Pre/post-processing:
  - ◆ Language for parameterized mesh description
  - ◆ Mainly use tied meshes of mapped blocks
  - ◆ MATLAB graphics, some ability to export to OpenDX
- Elements:
  - ◆ Isotropic and anisotropic scalar, elastic, TED elements
  - ◆ Linear, quadratic, and cubic shapes supported
  - ◆ All elements allow PML mapping
- Analyses:
  - ◆ Modal analysis: standard, PML, and TED
  - ◆ Forced response and energy flux computation
  - ◆ Model reduction and fast Bode plots
  - ◆ Parameter sweeps on any of the above

# Planned work

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- Short term
  - ◆ 3D calculations
  - ◆ Intrinsic material loss models
  - ◆ Piezo models?
  - ◆ Studies of grain boundary effects in TED
  - ◆ Continued comparisons to disk resonators
  - ◆ Comparisons to flextural resonator data
  - ◆ User documentation
  - ◆ Finding a new name!
- Long term
  - ◆ Computer optimization of bandpass filter designs
  - ◆ Continued simulation/verification of actual devices

# Conclusions

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- HiQLab page: [www.cs.berkeley.edu/~dbindel/hiqlab](http://www.cs.berkeley.edu/~dbindel/hiqlab)
- Questions or comments?