# Model Reduction and Mode Computation for Damped Resonant MEMS 

David Bindel

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## Collaborators

- Tsuyoshi Koyama
- Sanjay Govindjee
- Sunil Bhave
- Emmanuel Quévy
- Zhaojun Bai


## Resonant MEMS



Microguitars from Cornell University (1997 and 2003)

- MHz-GHz mechanical resonators
- Favorite application: radio on chip
- Close second: really high-pitch guitars


## The Mechanical Cell Phone



- Your cell phone has many moving parts!
- What if we replace them with integrated MEMS?


## Ultimate Success

## "Calling Dick Tracy!"



## Example Resonant System



## Example Resonant System



## The Designer's Dream

Ideally, would like

- Simple models for behavioral simulation
- Parameterized for design optimization
- Including all relevant physics
- With reasonably fast and accurate set-up

We aren't there yet. Today, some progress on the last two.

## Damping and $Q$

Designers want high quality of resonance ( $Q$ )

- Dimensionless damping in a one-dof system

$$
\frac{d^{2} u}{d t^{2}}+Q^{-1} \frac{d u}{d t}+u=F(t)
$$

- For a resonant mode with frequency $\omega \in \mathbb{C}$ :

$$
Q:=\frac{|\omega|}{2 \operatorname{lm}(\omega)}=\frac{\text { Stored energy }}{\text { Energy loss per radian }}
$$

## Damping Mechanisms

Possible loss mechanisms:

- Anchor loss
- Thermoelastic damping
- Other material losses
- Fluid damping

Our goal: Reduced models that include these effects.

## Perfectly Matched Layers



Model substrate as semi-infinite with a Perfectly Matched Layer (PML).

- Complex coordinate transformation
- Generates a "perfectly matched" absorbing layer
- Idea works with general linear wave equations


## Perfectly Matched Layers by Picture




Transformed coordinate


## Perfectly Matched Layers by Picture



Incoming $\exp (i \tilde{x})$


Transformed coordinate


## Perfectly Matched Layers by Picture

Outgoing $\exp (-i \tilde{x})$


Incoming $\exp (i \tilde{x})$


Transformed coordinate


## Perfectly Matched Layers by Picture




Transformed coordinate


## Perfectly Matched Layers by Picture




Transformed coordinate


## Perfectly Matched Layers by Picture




Transformed coordinate


## Finite Element Implementation





- Combine PML and isoparametric mappings

$$
\begin{aligned}
\mathbf{k}^{e} & =\int_{\Omega^{\square}} \tilde{\mathbf{B}}^{\top} \mathbf{D} \tilde{\mathbf{B}} \tilde{J} d \Omega^{\square} \\
\mathbf{m}^{e} & =\int_{\Omega^{\square}} \rho \mathbf{N}^{\top} \tilde{N} \tilde{J} d \Omega^{\square}
\end{aligned}
$$

- Matrices are complex symmetric


## Complex Symmetry

Discretized (forced) problem + fixed PML take the form:

$$
\left(K-\omega^{2} M\right) u=f, \text { where } K=K^{T}, M=M^{T}
$$

Can still characterize $u$ as a stationary point of

$$
I(u)=\frac{1}{2} u^{T}\left(K-\omega^{2} M\right) u-u^{T} f
$$

Eigenvalues of $(K, M)$ are stationary points of

$$
\rho(u)=\frac{u^{T} K u}{u^{T} M u}
$$

First-order accurate vectors $\Longrightarrow$ second-order accurate eigenvalues.

## Accurate Model Reduction

- Usual: Orthogonal projection onto Arnoldi basis V.
- Us: Build new projection basis from V:

$$
W=\operatorname{orth}[\operatorname{Re}(V), \operatorname{Im}(V)]
$$

- $\operatorname{span}(W)$ contains both $\mathcal{K}_{n}$ and $\overline{\mathcal{K}}_{n}$
$\Longrightarrow$ double digits correct vs. projection with $V$
- $W$ is a real-valued basis
$\Longrightarrow$ projected system is complex symmetric


## Model Reduction Accuracy



Results from ROM (solid and dotted lines) near indistinguishable from full model (crosses)

## Model Reduction Accuracy



Preserve structure $\Longrightarrow$ get twice the correct digits

## Thermoelastic Damping (TED)



## Thermoelastic Damping (TED)

$u$ is displacement and $T=T_{0}+\theta$ is temperature

$$
\begin{aligned}
\sigma & =\boldsymbol{C} \epsilon-\beta \theta 1 \\
\rho \ddot{u} & =\nabla \cdot \sigma \\
\rho \boldsymbol{c}_{V} \dot{\theta} & =\nabla \cdot(\kappa \nabla \theta)-\beta T_{0} \operatorname{tr}(\dot{\epsilon})
\end{aligned}
$$

- Coupling between temperature and volumetric strain:
- Compression and expansion $\Longrightarrow$ heating and cooling
- Heat diffusion $\Longrightarrow$ mechanical damping
- Not often an important factor at the macro scale
- Recognized source of damping in microresonators
- Zener: semi-analytical approximation for TED in beams
- We consider the fully coupled system


## Nondimensionalized Equations

Continuum equations:

$$
\begin{aligned}
\sigma & =\hat{C} \epsilon-\xi \theta 1 \\
\ddot{u} & =\nabla \cdot \sigma \\
\dot{\theta} & =\eta \nabla^{2} \theta-\operatorname{tr}(\dot{\epsilon})
\end{aligned}
$$

Discrete equations:

$$
\begin{aligned}
M_{u u} \ddot{u}+K_{u u} u & =\xi K_{u \theta} \theta+f \\
C_{\theta \theta} \ddot{\theta}+\eta K_{\theta \theta} \theta & =-C_{\theta u} \dot{u}
\end{aligned}
$$

- Micron-scale poly-Si devices: $\xi$ and $\eta$ are $\sim 10^{-4}$.
- Linearize about $\xi=0$


## Perturbative Mode Calculation

Discretized mode equation:

$$
\begin{aligned}
\left(-\omega^{2} M_{u u}+K_{u u}\right) u & =\xi K_{u \theta} \theta \\
\left(i \omega C_{\theta \theta}+\eta K_{\theta \theta}\right) \theta & =-i \omega C_{\theta u} u
\end{aligned}
$$

First approximation about $\xi=0$ :

$$
\begin{aligned}
\left(-\omega_{0}^{2} M_{u u}+K_{u u}\right) u_{0} & =0 \\
\left(i \omega_{0} C_{\theta \theta}+\eta K_{\theta \theta}\right) \theta_{0} & =-i \omega_{0} C_{\theta u} u_{0}
\end{aligned}
$$

First-order correction in $\xi$ :

$$
-\delta\left(\omega^{2}\right) M_{u u} u_{0}+\left(-\omega_{0}^{2} M_{u u}+K_{u u}\right) \delta u=\xi K_{u \theta} \theta_{0}
$$

Multiply by $u_{0}^{T}$ :

$$
\delta\left(\omega^{2}\right)=-\xi\left(\frac{u_{0}^{T} K_{u \theta} \theta_{0}}{u_{0}^{T} M_{u u} u_{0}}\right)
$$

## Zener's Model

(1) Clarence Zener investigated TED in late 30s-early 40s.
(2) Model for beams common in MEMS literature.
(3) "Method of orthogonal thermodynamic potentials" == perturbation method + a variational method.

## Comparison to Zener's Model



- Comparison of fully coupled simulation to Zener approximation over a range of frequencies
- Real and imaginary parts after first-order correction agree to about three digits with Arnoldi


## General Picture

If $w^{*} A=0$ and $A v=0$ then

$$
\delta\left(w^{*} A v\right)=w^{*}(\delta A) v
$$

This implies

- If $A=A(\lambda)$ and $w=w(v)$, have

$$
w^{*}(v) A(\rho(v)) v=0
$$

$\rho$ stationary when $(\rho(v), v)$ is a nonlinear eigenpair.

- If $A(\lambda, \xi)$ and $w_{0}^{*}$ and $v_{0}$ are null vectors for $A\left(\lambda_{0}, \xi_{0}\right)$,

$$
w_{0}^{*}\left(A_{\lambda} \delta \lambda+A_{\xi} \delta \xi\right) v_{0}=0
$$

## Conclusions

- Resonant MEMS have lots of interesting applications
- Designers want reduced models with relevant physics
- Damping is crucial, but not well handled in general
- Our work: use equation structure in making reduced models with damping (modal or more general)

