# Computer Aided Design of Micro-Electro-Mechanical Systems

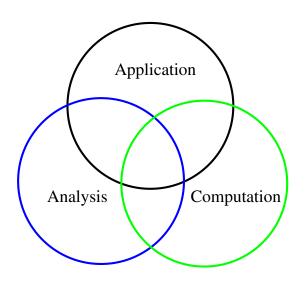
From Eigenvalues to Devices

David Bindel

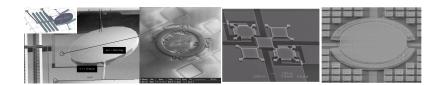
Department of Computer Science Cornell University

Duke University, 4 Apr 2013

# The Computational Science & Engineering Picture



# A Favorite Application: MEMS



#### I've worked on this for a while:

- SUGAR (early 2000s) SPICE for MEMS
- HiQLab (2006) high-Q mechanical resonator device modeling
- AxFEM (2012) solid-wave gyro device modeling

Goal today: two illustrative snapshots.

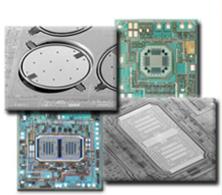
## Outline

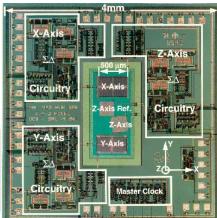
- Resonant MEMS
- 2 Anchor losses and disk resonators
- 3 Elastic wave gyros
- 4 Conclusion

#### **MEMS Basics**

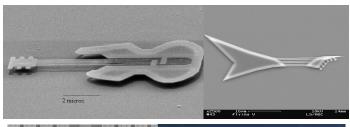
- Micro-Electro-Mechanical Systems
  - Chemical, fluid, thermal, optical (MECFTOMS?)
- Applications:
  - Sensors (inertial, chemical, pressure)
  - Ink jet printers, biolab chips
  - Radio devices: cell phones, inventory tags, pico radio
- Use integrated circuit (IC) fabrication technology
- Tiny, but still classical physics

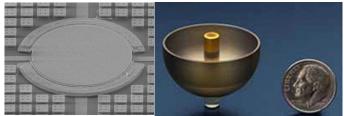
#### Where are MEMS used?





# My favorite applications

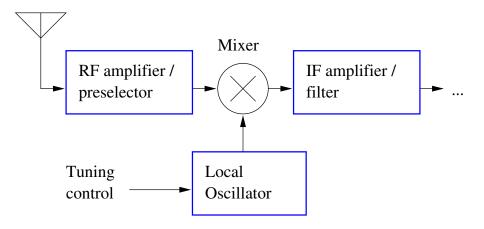




# Why you should care, too!



#### The Mechanical Cell Phone



...and lots of mechanical sensors, too!

### **Ultimate Success**

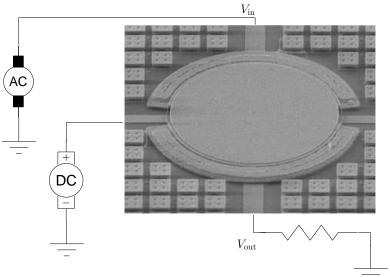
#### "Calling Dick Tracy!"



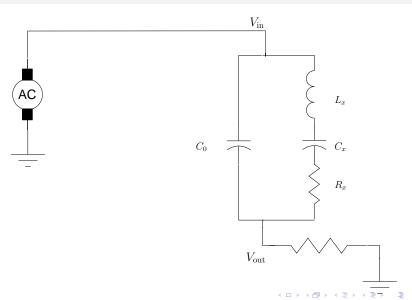
# **Computational Challenges**

Devices are fun – but I'm not a device designer. Why am I in this?

# Model System



# The Circuit Designer View



### Electromechanical Model

Balance laws ( KCL and BLM ):

$$\frac{d}{dt} (C(u)V) + GV = I_{\text{external}}$$

$$Mu_{tt} + Ku - \nabla_u \left(\frac{1}{2}V^*C(u)V\right) = F_{\text{external}}$$

Linearize about static equilibium  $(V_0, u_0)$ :

$$C(u_0) \, \delta V_t + G \, \delta V + (\nabla_u C(u_0) \cdot \delta u_t) \, V_0 = \delta I_{\text{external}}$$

$$M \, \delta u_{tt} + \tilde{K} \, \delta u + \nabla_u \left( V_0^* C(u_0) \, \delta V \right) = \delta F_{\text{external}}$$

where

$$\tilde{K} = K - \frac{1}{2} \frac{\partial^2}{\partial u^2} \left( V_0^* C(u_0) V_0 \right)$$

#### **Electromechanical Model**

Assume time-harmonic steady state, no external forces:

$$\begin{bmatrix} i\omega C + G & i\omega B \\ -B^T & \tilde{K} - \omega^2 M \end{bmatrix} \begin{bmatrix} \delta \hat{V} \\ \delta \hat{u} \end{bmatrix} = \begin{bmatrix} \delta \hat{I}_{\text{external}} \\ 0 \end{bmatrix}$$

Eliminate the mechanical terms:

$$Y(\omega) \, \delta \hat{V} = \delta \hat{I}_{\text{external}}$$
  
 $Y(\omega) = i\omega C + G + i\omega H(\omega)$   
 $H(\omega) = B^T (\tilde{K} - \omega^2 M)^{-1} B$ 

Goal: Understand electromechanical piece ( $i\omega H(\omega)$ ).

- As a function of geometry and operating point
- Preferably as a simple circuit

# Damping and Q

Designers want high quality of resonance (Q)

Dimensionless damping in a one-dof system

$$\frac{d^2u}{dt^2} + Q^{-1}\frac{du}{dt} + u = F(t)$$

• For a resonant mode with frequency  $\omega \in \mathbb{C}$ :

$$Q:=rac{|\omega|}{2\operatorname{Im}(\omega)}=rac{ ext{Stored energy}}{ ext{Energy loss per radian}}$$

To understand Q, we need damping models!

(Cornell University)

# The Designer's Dream

#### Reality is messy:

- Coupled physics
- ... some poorly understood (damping)
- ... subject to fabrication errors

#### Ideally, would like:

- Simple models for behavioral simulation
- Parameterized for design optimization
- Including all relevant physics
- With reasonably fast and accurate set-up

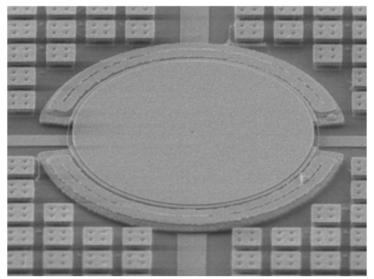
We aren't there yet.



#### **Outline**

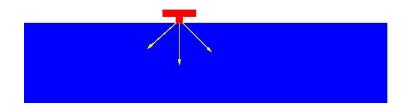
- Resonant MEMS
- Anchor losses and disk resonators
- Elastic wave gyros
- 4 Conclusion

#### **Disk Resonator Simulations**



(Cornell University) Fudan 19 / 55

# **Damping Mechanisms**



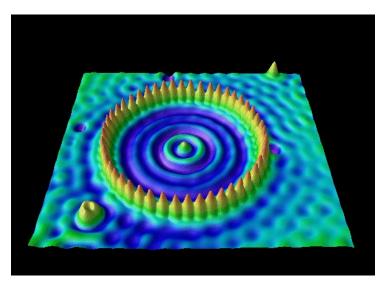
#### Possible loss mechanisms:

- Fluid damping
- Material losses
- Thermoelastic damping
- Anchor loss

Model substrate as semi-infinite ⇒ resonances!



# Resonances in Physics



#### Resonances and Literature



#### Listening to a Monk from Shu Playing the Lute

The monk from Shu with his green lute-case walked Westward down Emei Shan, and at the sound Of the first notes he strummed for me I heard A thousand valleys' rustling pines resound. My heart was cleansed, as if in flowing water. In bells of frost I heard the resonance die. Dusk came unnoticed over the emerald hills And autumn clouds layered the darkening sky.

Chinese Poems on the Underground

Li Bai (AD 701-761) Translated by Wimm Seth. Three Orleans Peets Obtain: 1982)
Oil sprainly by Qui Lei Lei
A cultural exchange between Shanghai Metro and London Underground



MAYOR OF LONDON







ansport for London

4 = 3 + 4 = 3 + 4 = 3 +

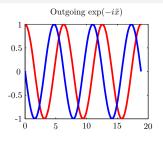


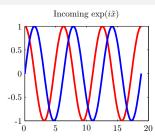
In bells of frost I heard the resonance die.

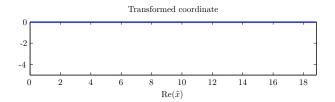
Li Bai (translated by Vikram Seth)

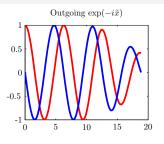
# Perfectly Matched Layers

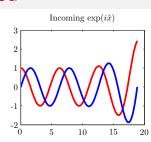
- Complex coordinate transformation
- Generates a "perfectly matched" absorbing layer
- Idea works with general linear wave equations
  - Electromagnetics (Berengér, 1994)
  - Quantum mechanics exterior complex scaling (Simon, 1979)
  - Elasticity in standard finite element framework (Basu and Chopra, 2003)
  - Works great for MEMS, too! (Bindel and Govindjee, 2005)

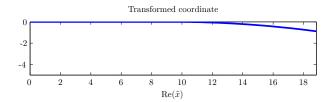


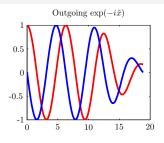


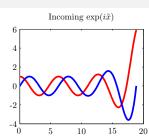


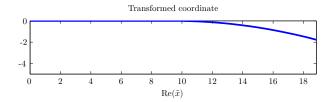


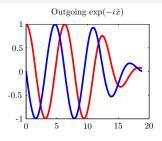


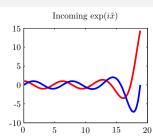


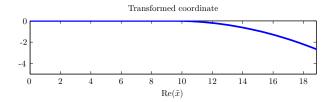


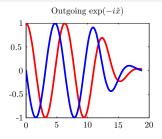


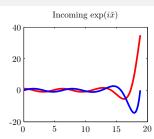


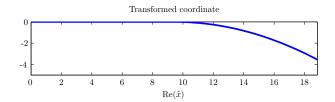


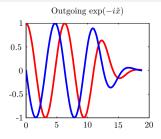


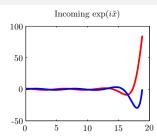


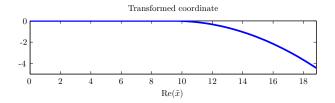




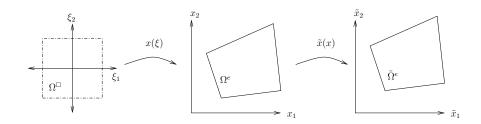






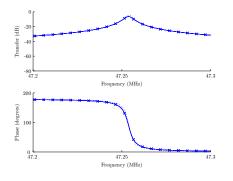


# Finite Element Implementation



Matrices are complex symmetric

# Eigenvalues and Model Reduction



Goal: understand  $H(\omega)$ :

$$H(\omega) = B^T (K - \omega^2 M)^{-1} B$$

Look at

- Poles of H (eigenvalues)
- Bode plots of H

*Model reduction*: Replace  $H(\omega)$  by cheaper  $\hat{H}(\omega)$ .

# Approximation from Subspaces

A general recipe for large-scale numerical approximation:

- **1** A subspace V containing good approximations.
- ② A criterion for "optimal" approximations in  $\mathcal{V}$ .

Basic building block for eigensolvers and model reduction!

Better subspaces, better criteria, better answers.

# Variational Principles

- Variational form for complex symmetric eigenproblems:
  - Hermitian (Rayleigh quotient):

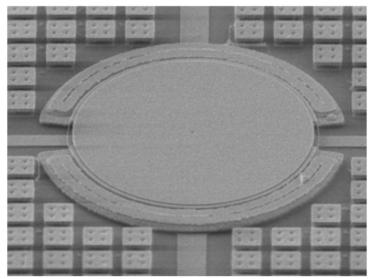
$$\rho(v) = \frac{v^* K v}{v^* M v}$$

Complex symmetric (modified Rayleigh quotient):

$$\theta(v) = \frac{v^T K v}{v^T M v}$$

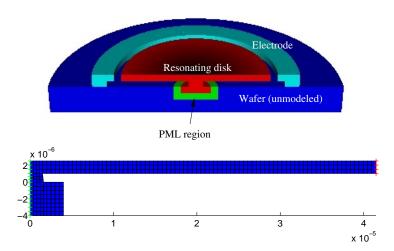
- Good for model reduction, too!

#### **Disk Resonator Simulations**



(Cornell University) Fudan 29 / 55

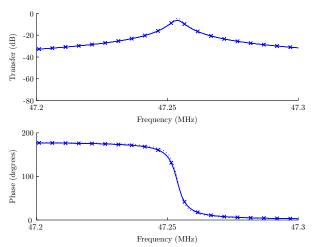
#### **Disk Resonator Mesh**



Axisymmetric model, bicubic,  $\approx 10^4$  nodal points at convergence

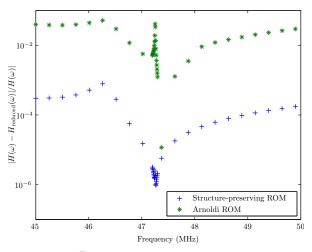
4 中 x 4 图 x 4 图 x 4 图 x

# Model Reduction Accuracy



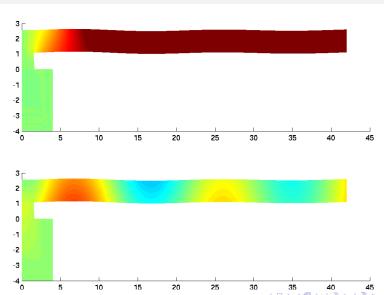
Results from ROM (solid and dotted lines) nearly indistinguishable from full model (crosses)

## **Model Reduction Accuracy**

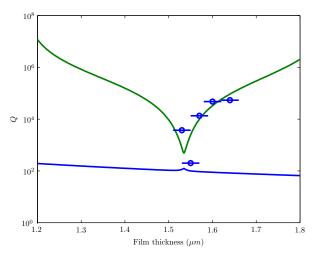


Preserve structure ⇒ get twice the correct digits

## Response of the Disk Resonator

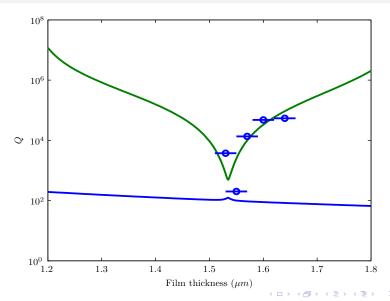


## Variation in Quality of Resonance

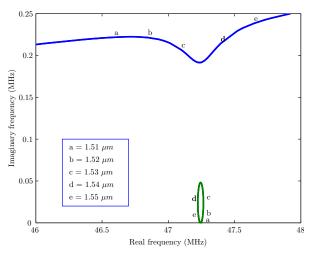


Simulation and lab measurements vs. disk thickness

# Explanation of ${\it Q}$ Variation



## Explanation of Q Variation



Interaction of two nearby eigenmodes

### Outline

- Resonant MEMS
- 2 Anchor losses and disk resonators
- Elastic wave gyros
- 4 Conclusion

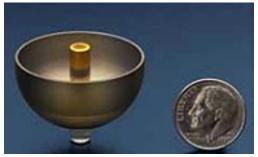
## Bryan's Experiment





"On the beats in the vibrations of a revolving cylinder or bell" by G. H. Bryan, 1890

## A Small Application



Northrup-Grummond HRG

## Current example: Micro-HRG / GOBLiT / OMG

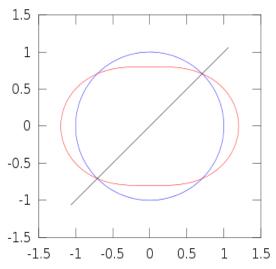


(Cornell University)

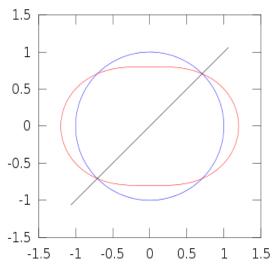


- Goal: Cheap, small (1mm) HRG
- Collaborator roles:
  - Basic design
  - Fabrication
  - Measurement
- Our part:
  - Detailed physics
  - Fast software
  - Sensitivity
  - Design optimization

## How It Works



## How It Works



### Goal state

### We want to compute:

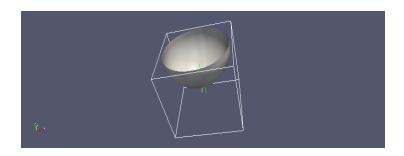
- Geometry
- Fundamental frequencies
- Angular gain (Bryan's factor)
- Damping (thermoelastic, radiation, material)
- Sensitivities of everything
- Effects of symmetry breaking

### For speed and accuracy: use structure!

- Axisymmetric geometry ⇒ 3D to 2D via Fourier
- Perturbed geometry 

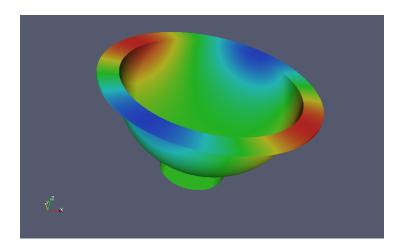
  interactions for different wave numbers

## Getting the Geometry



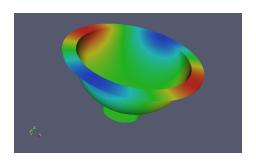
- Simple isotropic etch modeling fails 1mm is huge!
- Working on better simulator (reaction-diffusion).
- For now, take idealized geometries on faith...

# Full Dynamics



45 / 55

## **Essential Dynamics**



Dynamics in 2D subspace of degenerate modes:

$$\left(-\omega^2 mI + 2i\omega\Omega gJ + kI\right)c = 0$$

Scaled gain g is *Bryan's factor* 

 $\mathrm{BF} = \frac{\text{Angular rate of pattern relative to body}}{\text{Angular rate of vibrating body}}$ 

If no parameters in the world were very large or very small, science would reduce to an exhaustive list of everything.

— Nick Trefethen

### **Fourier Picture**

Write displacement fields as Fourier series:

$$\mathbf{u} = \sum_{m=0}^{\infty} \left( \begin{bmatrix} u_{mr}(r,z)\cos(m\theta) \\ u_{m\theta}(r,z)\sin(m\theta) \\ u_{mz}(r,z)\cos(m\theta) \end{bmatrix} + \begin{bmatrix} -u'_{mr}(r,z)\sin(m\theta) \\ u'_{m\theta}(r,z)\cos(m\theta) \\ -u'_{mz}(r,z)\sin(m\theta) \end{bmatrix} \right)$$

- Works whenever geometry is axisymmetric
- Treat non-axisymmetric geometries as mapped axisymmetric
  - Now coefficients in PDEs are non-axisymmetric
- ullet Problems with different m decouple if *everything* axisymmetric

### **Fourier Picture**

### Perfect axisymmetry:

$$\begin{bmatrix} K_{11} & & & & & \\ & K_{22} & & & & \\ & & K_{33} & & \\ & & & \ddots \end{bmatrix} - \omega^2 \begin{bmatrix} M_{11} & & & & \\ & M_{22} & & & \\ & & & M_{33} & \\ & & & & \ddots \end{bmatrix}$$

### **Fourier Picture**

### Broken symmetry (via coefficients):

$$\begin{bmatrix} K_{11} & \epsilon & \epsilon & \epsilon \\ \epsilon & K_{22} & \epsilon & \epsilon \\ \epsilon & \epsilon & K_{33} & \epsilon \\ \epsilon & \epsilon & \epsilon & \cdot \cdot \end{bmatrix} - \omega^2 \begin{bmatrix} M_{11} & \epsilon & \epsilon & \epsilon \\ \epsilon & M_{22} & \epsilon & \epsilon \\ \epsilon & \epsilon & M_{33} & \epsilon \\ \epsilon & \epsilon & \epsilon & \cdot \cdot \end{bmatrix}$$

## Perturbing Fourier

Modes "near" azimuthal number m = nonlinear eigenvalues

$$\left(K_{mm} - \omega^2 M_{mm} + E_{mm}(\omega)\right) u = 0.$$

#### Need:

- Control on  $E_{mm}$ 
  - Depends on frequency spacing
  - Depends on Fourier analysis of perturbation
- Perturbation theory for nonlinearly perturbed eigenproblems
  - For self-adjoint case, results similar to Lehmann intervals

First-order estimate:  $(K_{mm} - \omega_0^2 M_{mm}) u_0 = 0$ ; then

$$\delta(\omega^2) = \frac{u_0^T E_{mm}(\omega_0) u_0}{u_0^T M_{mm} u_0}.$$

### Perturbation and Radiation

Incorporating numerical radiation BCs gives:

$$\left( K - \omega^2 M + G(\omega) \right) u = 0.$$

Perturbation approach: ignore G to get  $(\omega_0, u_0)$ . Then

$$\delta(\omega^2) = \frac{u_0^T G(\omega_0) u_0}{u_0^T M_{mm} u_0}.$$

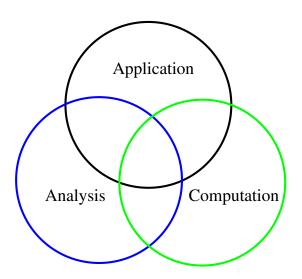
Works when BC has small influence (coefficients aren't small).

Also an approach to understanding sensitivity to BC!
... explains why PML works okay despite being inappropriate?

### Outline

- Resonant MEMS
- 2 Anchor losses and disk resonators
- Blastic wave gyros
- Conclusion

## The Computational Science & Engineering Picture



### Conclusions

The difference between art and science is that science is what we understand well enough to explain to a computer. Art is everything else.

Donald Knuth

The purpose of computing is insight, not numbers.
Richard Hamming

- Collaborators:
  - Disk: S. Govindjee, T. Koyama, S. Bhave, E. Quevy
  - HRG: S. Bhave, L. Fegely, E. Yilmaz
- Funding: DARPA MTO, Sloan Foundation